

NUCLEAR WEAPONS EFFECTS

HANDBOOK

A collection of the graphs, nomograms,
and tabulated data most frequently used
by the Radiological Scientific Officer.

PREFACE

This handbook was compiled in an effort to simplify the use of the basic text used on Radiological Scientific Officers courses, i.e., The Effects of Nuclear Weapons, 1962 (reprint edition, 1964).

The Effects of Nuclear Weapons is an excellent reference book and will continue to be used for RSO courses. However, students have frequently commented upon the difficulty of quickly locating the graphs and tables which they regularly use for preparing their weapons effects estimates; a single computation may require reference to several graphs, each located in a different chapter in the text. Therefore, those data most frequently used by the RSO have been extracted from The Effects of Nuclear Weapons and re-assembled in this handbook in subject groups more closely related to the normal order of use.

To complete the usefulness of this handbook, data from one or two other sources have been inserted in some sections and a full section of "useful relationships", containing selected mathematical tables, conversion factors, etc., is included.

Users must remember that this handbook contains only selected data; it is not a full and complete manual of nuclear weapons effects. It must be used therefore, in conjunction with its source documents, in which the various phenomena are discussed and explained and which define or qualify the order of reliability of some of the data.

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SECTION A - BLAST & SHOCK

A-1 AIR BLAST

Figures 3.67a & b. Peak overpressures on the ground for a 1-kiloton burst (high and low-pressure ranges)

The curves in Figs. 3.67a & b show peak overpressures on the ground as a function of distance from ground zero and height of burst for a 1 KT burst in a standard sea-level atmosphere. The broken line separates the regular reflection region from the Mach region and indicates where the triple point is formed. The data are considered appropriate to nearly-ideal target conditions.

SCALING:

The height of burst and the distance from ground zero to which a given peak overpressure extends scale as the cube root of the yield, i.e.,

$$\frac{d}{d_1} = \frac{h}{h_1} = W^{1/3}$$

where, for a given overpressure, d_1 and h_1 are distance from ground zero and height of burst for 1 KT and d and h are the corresponding distance and height of burst for W KT.

METHOD:

Given the yield W and any two of height of burst h , overpressure p , or distance d , to find the unknown, proceed as follows.

To find distance.

1. Calculate scaled height of burst: $h_1 = \frac{h}{W^{1/3}}$

2. From Fig. 3.67a or b, using scaled height h_1 and the given overpressure p , determine the scaled distance d_1 at which p is produced.

3. Convert scaled distance to actual distance: $d = d_1 W^{1/3}$

To find overpressure:

1. Calculate scaled height as above.

2. Calculate scaled distance: $d_1 = \frac{d}{W^{1/3}}$

3. Using h_1 and d_1 , read off p from Fig. 3.67a or b.

To find height of burst:

1. Calculate scaled distance as above.

2. From Fig. 3.67a or b, using d_1 and p , read off scaled height h_1 .

3. Convert scaled height to actual height: $h = h_1 W^{1/3}$

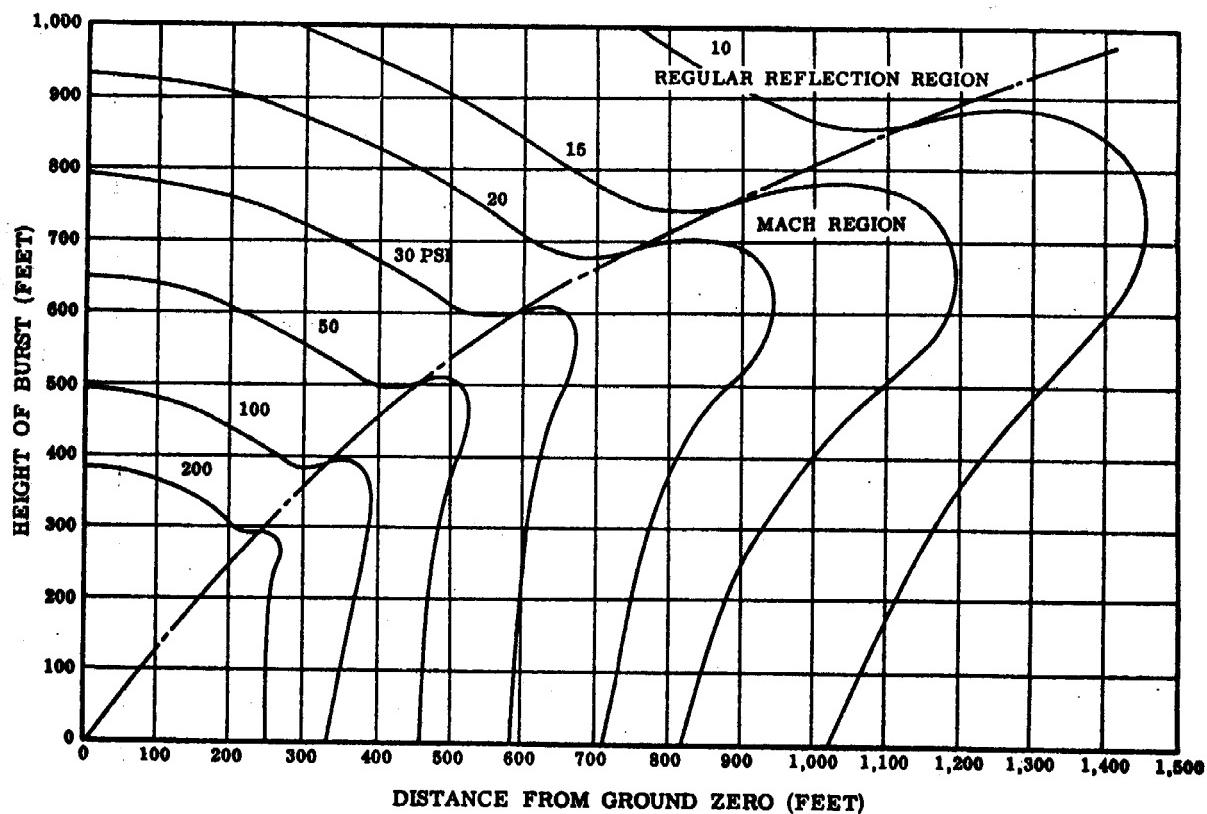


Figure 3.67a. Peak overpressures on the ground for a 1-kiloton burst (high-pressure range).

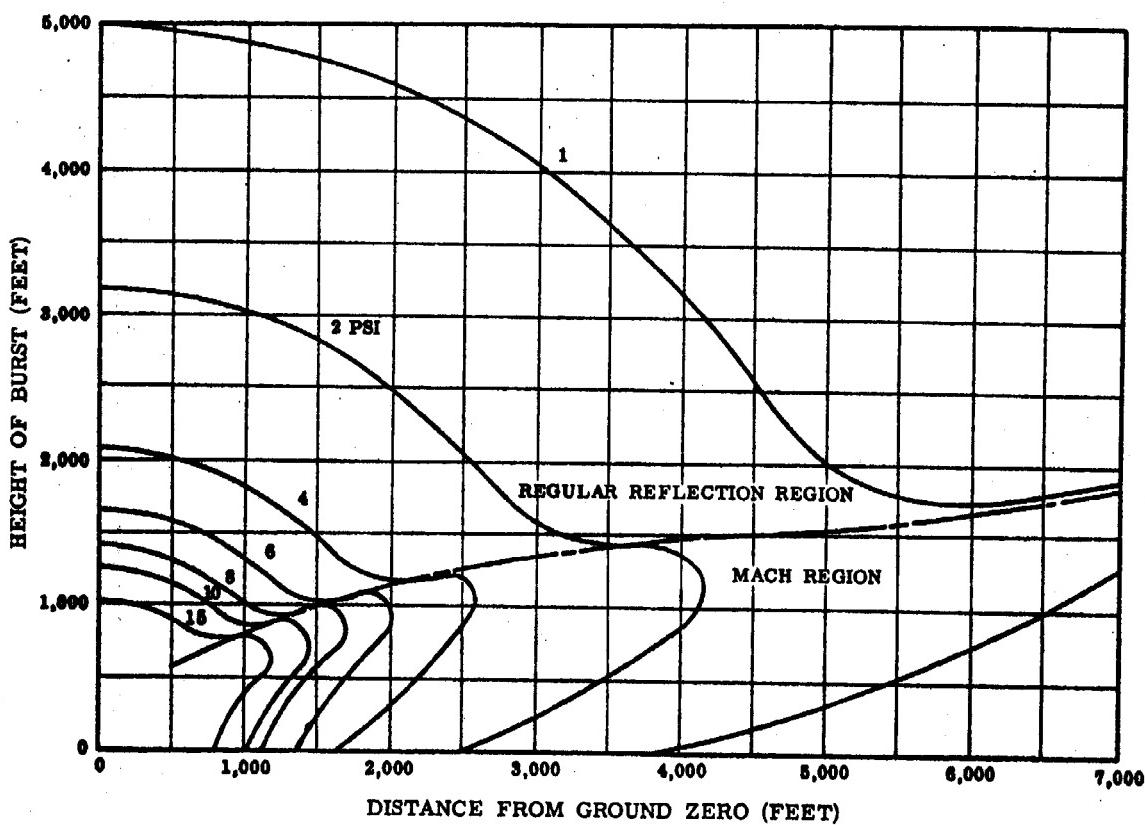


Figure 3.67b. Peak overpressures on the ground for 1-kiloton burst (low-pressure range).

(from Effects of Nuclear Weapons, 1964, pp 137, 139)

Figure 3.68. Horizontal component of peak dynamic pressure for 1-kiloton burst.

The curves in Fig. 3.68 show the horizontal component of peak dynamic pressure on the ground as a function of distance from ground zero and height of burst for a 1 KT burst in a standard sea-level atmosphere. The data are considered appropriate for nearly-ideal target conditions.

SCALING: as for Figs. 3.67a & b.

Figure 3.69. Positive phase duration on the ground of overpressure and dynamic pressure for 1-kiloton burst.

The curves in Fig. 3.69 show the duration on the ground of the positive phase of the overpressure and of the dynamic pressure (in parentheses) as a function of distance from ground zero and height of burst in a standard sea-level atmosphere. The curves are considered appropriate for nearly-ideal surface conditions.

SCALING:

The required relationships are $\frac{d}{d_1} = \frac{h}{h_1} = \frac{t}{t_1} = W^{1/3}$

where d_1 , h_1 , and t_1 , are the distance from ground zero, the height of burst, and duration, respectively, for 1 KT; and d , h , and t are the corresponding distance, height of burst, and duration for W KT.

EXAMPLE:

GIVEN: A 160 KT explosion at a height of 3,000 feet.

FIND: The positive phase duration on the ground of (a) the overpressure, (b) the dynamic pressure at 4,000 feet.

SOLUTION: The corresponding height of burst for 1 KT is

$$h_1 = \frac{h}{W^{1/3}} = \frac{3,000}{(160)^{1/3}} = 550 \text{ feet},$$

and the corresponding distance from ground zero is

$$d_1 = \frac{d}{W^{1/3}} = \frac{4,000}{(160)^{1/3}} = 740 \text{ feet}$$

(a) From Fig. 3.69, the positive phase duration of the overpressure for a 1 KT at 740 feet from ground zero and a burst height of 550 feet is 0.18 second. The corresponding duration of the overpressure positive phase for 160 KT is, therefore,

$$t = t_1 W^{1/3} = 0.18 \times (160)^{1/3} = 1.0 \text{ second ANSWER}$$

(b) From Fig. 3.69, the positive phase duration of the dynamic pressure for 1 KT at 740 feet from ground zero and a burst height of 550 feet is 0.34 second. The corresponding duration of the dynamic pressure positive phase for 160 KT is, therefore,

$$t = t_1 W^{1/3} = 0.34 \times (160)^{1/3} = 1.8 \text{ second ANSWER}$$

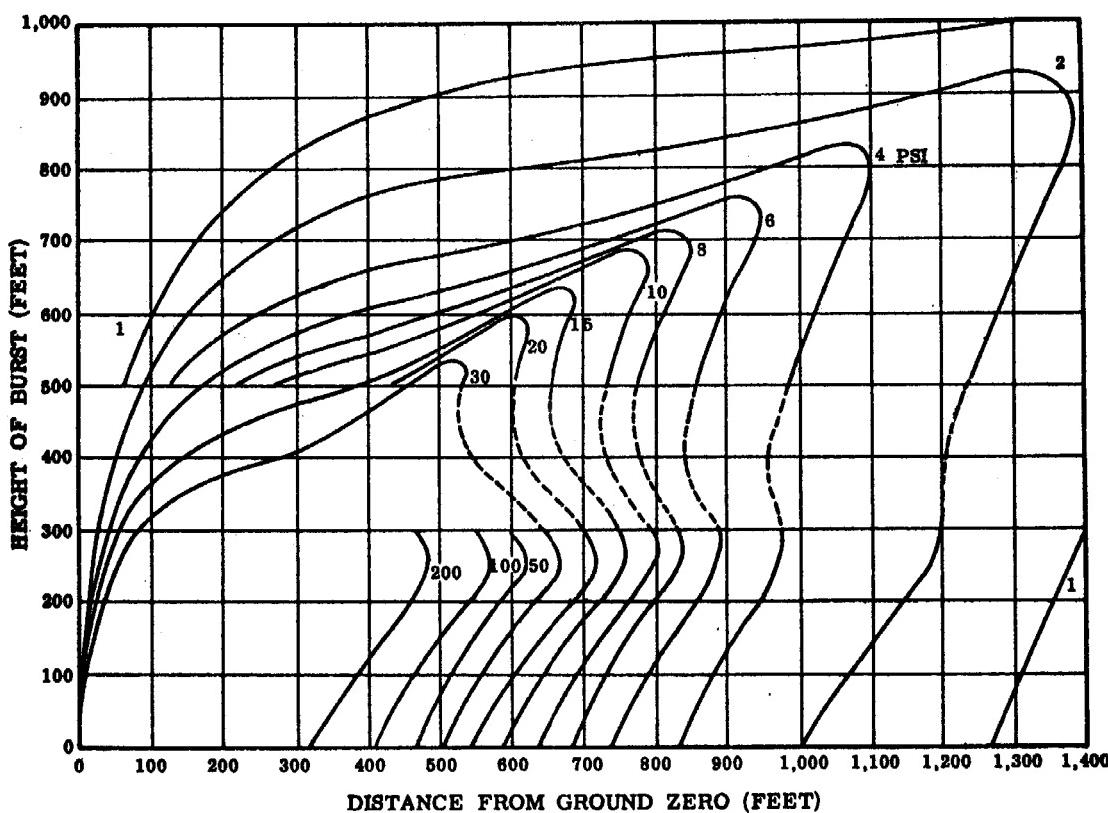


Figure 3.68. Horizontal component of peak dynamic pressure for 1-kiloton burst.

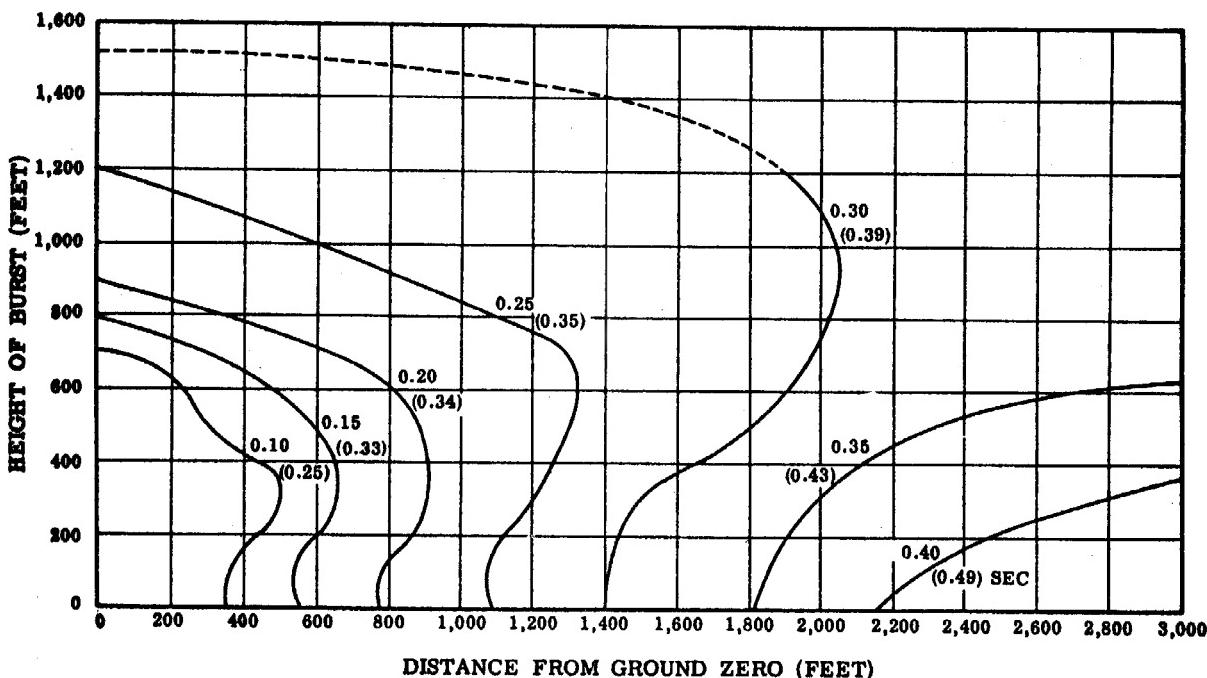


Figure 3.69. Positive phase duration on the ground of overpressure and dynamic pressure (in parentheses) for 1-kiloton burst.

(from Effects of Nuclear Weapons, 1964, pp 141, 143)

Figures 3.70a and b. Arrival times on the ground of blast wave for a 1-kiloton burst.

The curves in Figs. 3.70a & b give the time of arrival of the blast wave on the ground as a function of distance from ground zero and height of burst for a 1 KT burst in a standard sea-level atmosphere. The curves are considered appropriate for nearly-ideal surface conditions.

SCALING:

The required relationships are

$$\frac{d}{d_1} = \frac{h}{h_1} = \frac{t}{t_1} = W^{1/3}$$

where d_1 , h_1 , and t_1 are the distance from ground zero, height of burst, and time of arrival, respectively, for 1 KT; and d , h , and t are the corresponding distance height of burst, and time for W KT.

EXAMPLE:

GIVEN: A 1 MT explosion at a height of 5,000 feet.

FIND: The time of arrival of the blast wave at a distance of 10 miles from ground zero.

SOLUTION: The corresponding burst height for 1 KT is

$$h_1 = \frac{h}{W^{1/3}} = \frac{5,000}{(1,000)^{1/3}} = 500 \text{ feet}$$

The corresponding distance from ground zero for 1 KT is

$$d_1 = \frac{d}{W^{1/3}} = \frac{5,280 \times 10}{(1,000)^{1/3}} = 5,280 \text{ feet}$$

From Fig. 3.70b, at a height of burst of 500 feet and a distance of 5,280 feet from ground zero, the arrival time is 4.0 seconds for 1 KT.

The corresponding arrival time for 1 MT is

$$t = t_1 W^{1/3} = 4.0 \times (1,000)^{1/3} = 40 \text{ seconds ANSWER}$$

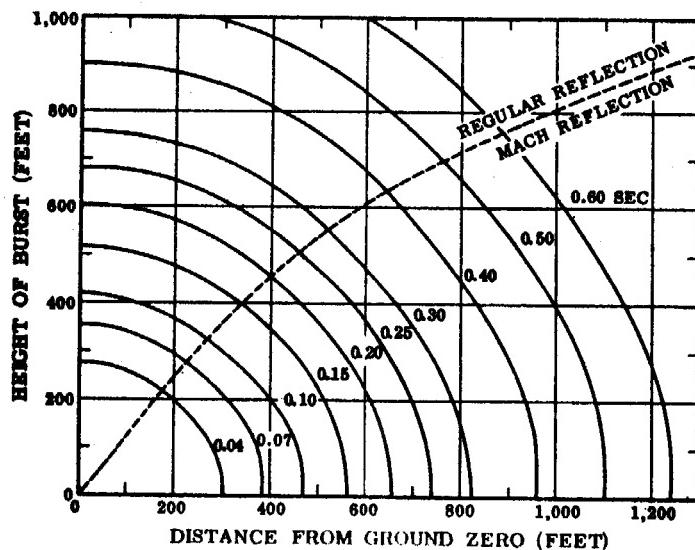


Figure 3.70a. Arrival times on the ground of blast wave for 1-kiloton burst (early times).

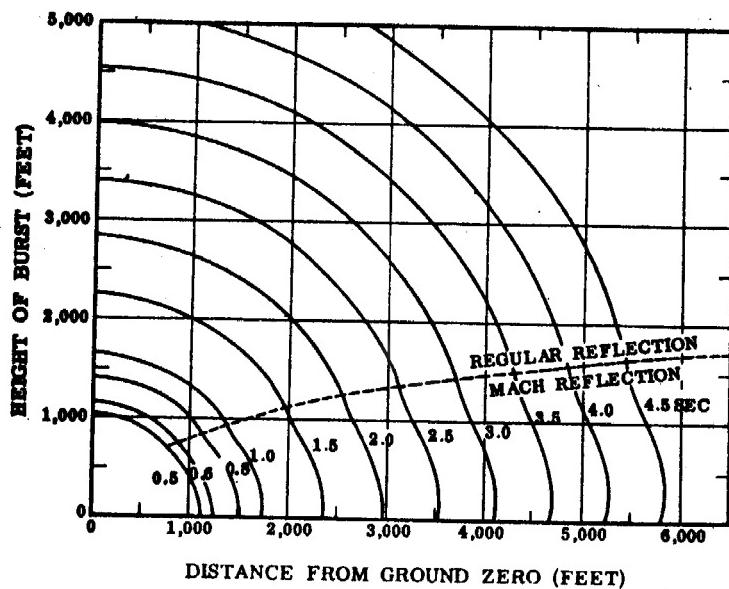


Figure 3.70b. Arrival times on the ground of blast wave for 1-kiloton burst (late times).

(from Effects of Nuclear Weapons, 1964, p 145)

SECTION A - BLAST & SHOCK

A-2 SURFACE & SUB-SURFACE BURSTS

A - 2

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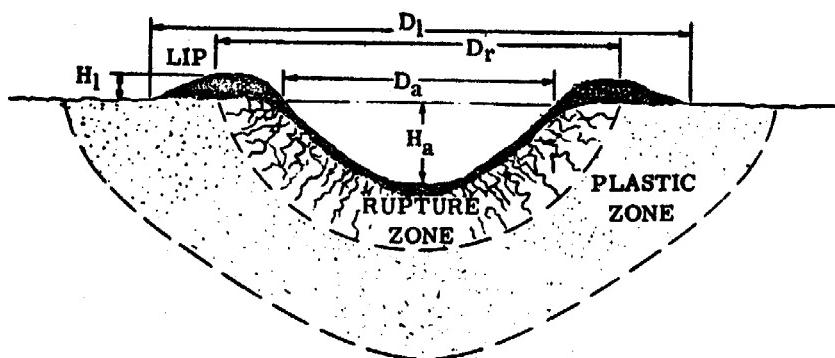


Figure 6.46. Characteristic dimensions of the crater in a surface burst.

The apparent crater, which has a diameter D_a and a depth H_a , as shown in Fig. 6.46, is the surface of the depression or hole left in the ground after the explosion. The true crater, diameter D_t , on the other hand, is the surface extending beyond the apparent crater where a definite shear has occurred.

The volume of the apparent crater, assumed to be roughly paraboloid, is given approximately by

$$\text{Volume of crater} = \frac{\pi D_a^2 H_a}{8}.$$

The diameter of the rupture zone, indicated by D_r in Fig. 6.46, is roughly one and one-half times the apparent crater diameter, i.e.,

$$D_r \approx 1.5 D_a.$$

The overall diameter, including the lip, i.e., D_L , is twice the apparent crater diameter, so that

$$D_L \approx 2D_a.$$

The height of the lip, H_L , is approximately one-fourth of the depth of the apparent crater, i.e.,

$$H_L \approx 0.25 H_a.$$

(from Effects of Nuclear Weapons, 1964, pp 289, 290)

Figure 6.48. Apparent crater dimensions for bursts at the surface and at a depth of $150 W^{0.3}$ feet in dry soil.

The curves in Fig. 6.48 give the values of apparent crater diameter and depth in dry soil as a function of explosion yield for (a) a surface burst, i.e., actual depth $5 W^{1/3}$ feet above or below the ground, and (b) a burst at an actual depth of $150 W^{0.3}$ feet. These curves represent the range in crater dimensions from a surface burst to the (approximate) maximum value for an underground burst.

A factor of 0.8 is used as a multiplier for estimating crater dimensions in rock, e.g., granite or sandstone.

EXAMPLE:

GIVEN: A 20 KT surface burst over sandstone.

FIND: The crater diameter and depth.

SOLUTION: From Fig. 6.48, the crater radius and depth for a 20 KT surface burst in dry soil are 170 feet and 80 feet, respectively. By applying the factor for sandstone (0.8), the estimated (approximate) crater dimensions are:

$$\text{Crater Diameter } (D_a) = 340 \times 0.8 = 270 \text{ feet}$$

$$\text{Crater Depth } (H_a) = 80 \times 0.8 = 64 \text{ feet ANSWER}$$

Figure 6.49. Apparent crater radius and depth as function of depth of burst for a 1-kiloton underground explosion in dry soil

The solid curves in Fig. 6.49 give the estimated apparent crater radius and depth as a function of depth of burst for 1 KT explosions in dry soil. The dashed curves indicate the reasonable range of variations to be expected under apparently similar conditions. For rock the multiplication factor of 0.8 should be used. The curves are uncertain at depths of burst greater than $150 W^{0.3}$ feet.

SCALING:

To determine the crater radius and depth for a W KT yield, the actual burst depth is divided by $W^{0.3}$ to obtain the scaled depth. The radius and depth of crater for 1 KT at this depth of burst are obtained from Fig. 6.49. The dimensions are then multiplied by $W^{0.3}$. (Values of $W^{0.3}$ can be obtained from Figure 3.65, which is reproduced in Section E-1 of this handbook.)

EXAMPLE:

GIVEN: A 20 KT burst at a depth of 50 feet in granite.

FIND: Crater radius and depth.

SOLUTION: The scaled burst depth is

$$\frac{d}{W^{0.3}} = \frac{50}{20^{0.3}} = \frac{50}{2.46} = 20 \text{ feet.}$$

From Fig. 6.49 the crater radius for a 1 KT explosion at this depth is 117 feet. The corresponding depth of the crater is 55 feet. Hence, the crater radius and depth for a 20 KT burst at a depth of 50 feet in granite are:

$$\text{Crater Radius } (R_a) = 117 \times 20^{0.3} \times 0.8 = 230 \text{ feet}$$

$$\text{Crater Depth } (H_a) = 55 \times 2.46 \times 0.8 = 108 \text{ feet ANSWER}$$

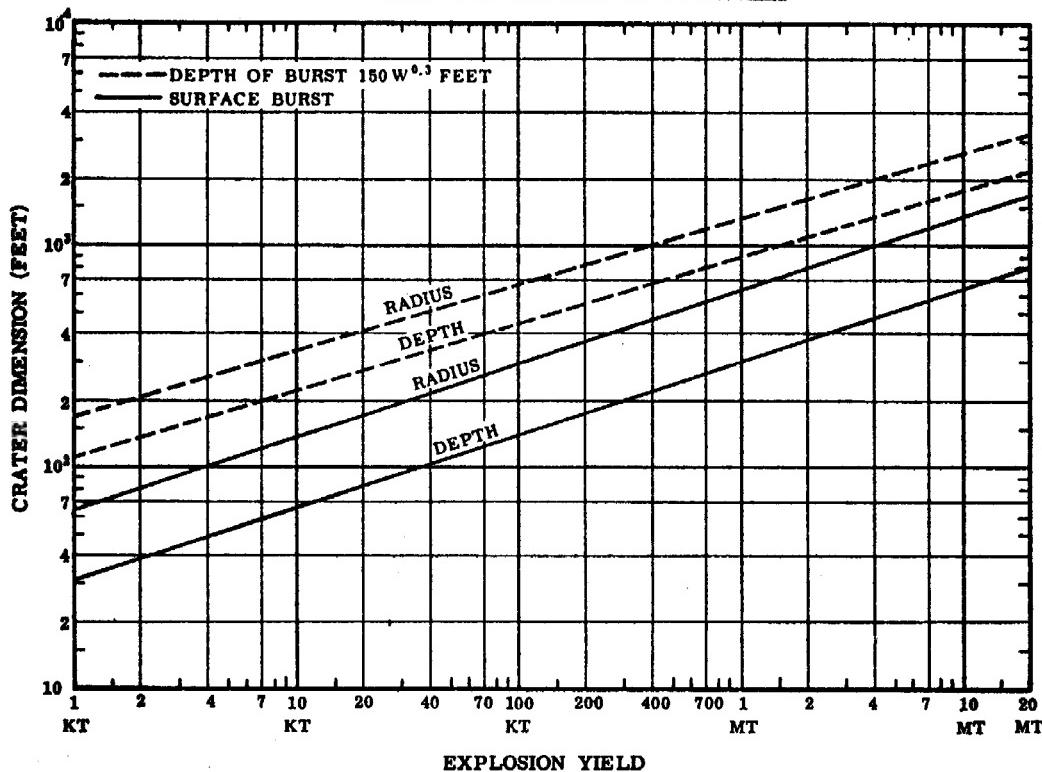


Figure 6.48. Apparent crater dimensions for bursts at the surface and at a depth of $150 W^{0.3}$ feet in dry soil.

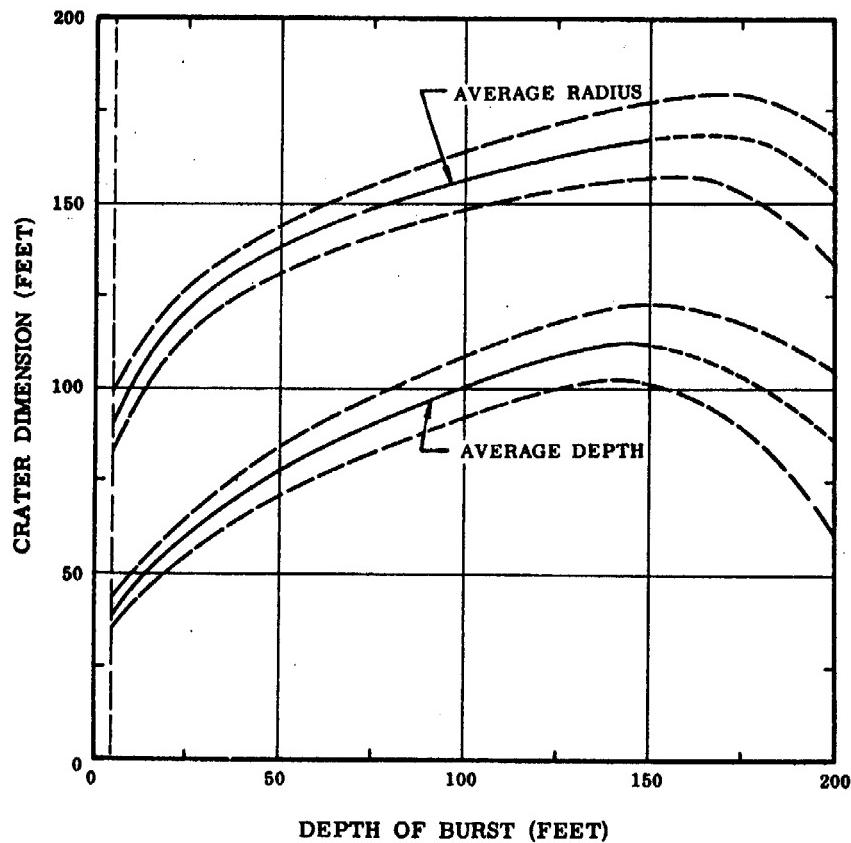


Figure 6.49. Apparent crater radius and depth as function of depth of burst for a 1-kiloton underground explosion in dry soil. (The data are uncertain for scaled depths of burst greater than 150 feet.)

(from Effects of Nuclear Weapons, 1964, pp 293, 295)

Figure 6.81. Dimensions of crater in underwater bursts as function of explosion yield.

The curves in Fig. 6.81 give the depth, diameter, and lip height of the underwater crater as functions of yield. The results are for a burst less than 15 feet deep and for one on the bottom in 50 feet of water for sand, sand and gravel, or soft rock bottom.

For other bottom materials the crater dimensions can be estimated by multiplying the values from Fig. 6.81 by the following factors:

<u>Material</u>	<u>Diameter</u>	<u>Depth</u>	<u>Lip Height</u>
Loess.....	1.0	1.7	0.7
Clay.....	1.0	2.3	2.3
Hard Rock.....	0.7	0.5	0.4
Mud or Muck.....	0.7	0.4	0.2

EXAMPLE:

GIVEN: A 200 KT weapon detonated in 50 feet of water; the bottom is predominately clay.

FIND: (a) The crater dimensions when the detonation is near the surface of the water.
 (b) The crater dimensions when the detonation occurs on the bottom.

SOLUTION: From Fig. 6.81, the crater dimensions for a 200 KT explosion are as follows:

	(a) feet	(b) feet
Diameter.....	1,000	1,900
Depth	44	120
Lip Height.....	2.4	14

For a clay bottom, the multiplication factors are 1.0 for the diameter, and 2.3 for both the depth and lip height; hence, the required values are:

	(a) feet	(b) feet
Diameter (factor 1.0).....	1,000	1,900
Depth (factor 2.3).....	100	276
Lip Height (factor 2.3).....	5.5	32

ANSWER

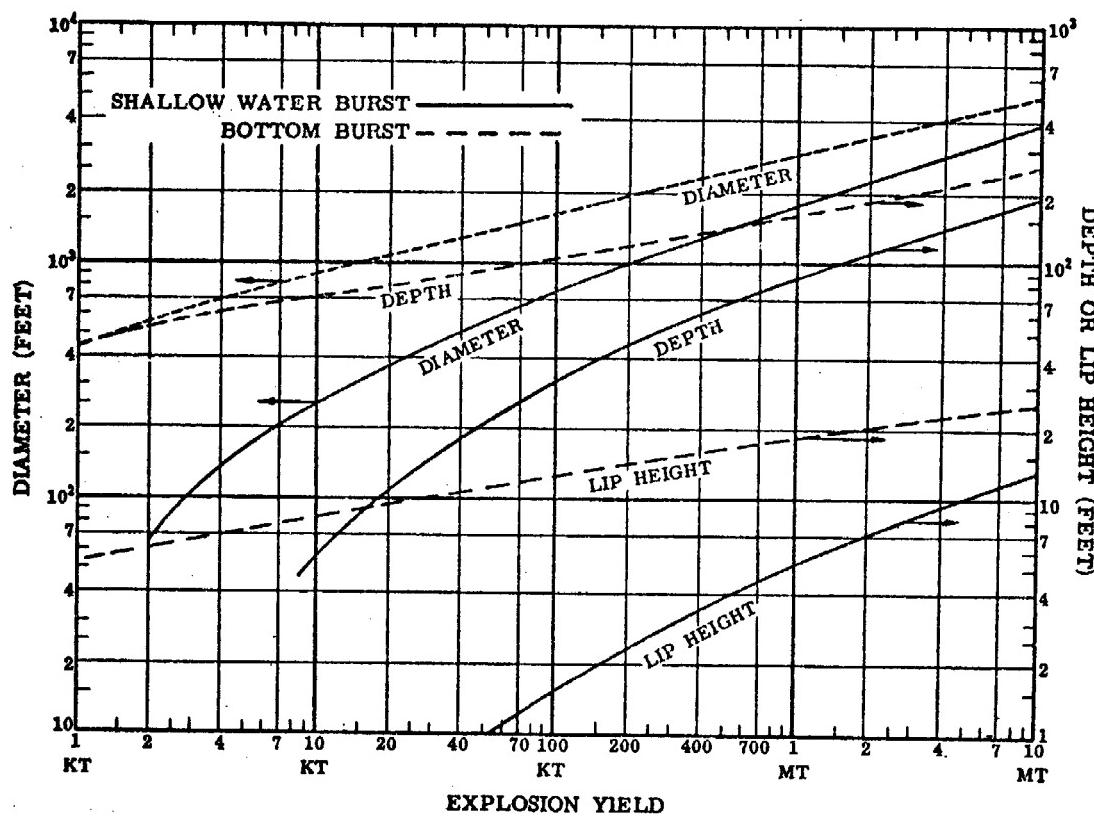


Figure 6.81. Dimensions of crater in underwater bursts as a function of explosion yield.

(from Effects of Nuclear Weapons, 1964, p 313)

Figure 6.79. Maximum wave height in different types of 1-kiloton under-water bursts.

The lower curve in Fig. 6.79 shows the approximate maximum crest-to-trough wave height versus horizontal surface distance for a 1 KT burst in water 85 feet deep. The upper curve is for a 1 KT burst in water more than 400 feet deep, so that the bottom does not affect the mechanism of wave formation.

SCALING:

At a given distance from surface zero, the wave height for an explosion of W kilotons is $W^{\frac{1}{2}}$ times the wave height at this distance from a 1 KT burst in water of the same scaled depth. The scaled depth is $d/W^{\frac{1}{4}}$, where d is the actual depth in feet. For the lower curve in the figure the scaled depth is 85 feet and for the upper curve it is more than 400 feet.

For scaled water depths less than 85 feet, i.e., actual depths less than $85 W^{\frac{1}{2}}$ feet, the estimated maximum wave height is proportional to the depth of the water.

METHOD:

Wave height is, therefore, scaled as follows:

- (1) Calculate scaled depth of water, using

$$d_1 = \frac{d}{W^{\frac{1}{4}}}$$

where, d_1 is scaled depth of water in feet,
 d is actual depth of water in feet, and
 W is yield in kilotons.

- (2) Select appropriate curve in Fig. 6.79 and read off scaled wave height h_1 for actual distance R .
- (3) Multiply scaled wave height h_1 by $W^{\frac{1}{2}}$
 - (a) For deep water (>85 scaled feet) this gives the estimated wave height h .
 - (b) In shallow water (<85 scaled feet) multiply h from step 3 by

$$\frac{d_1}{85}$$

to obtain the estimated wave height h .

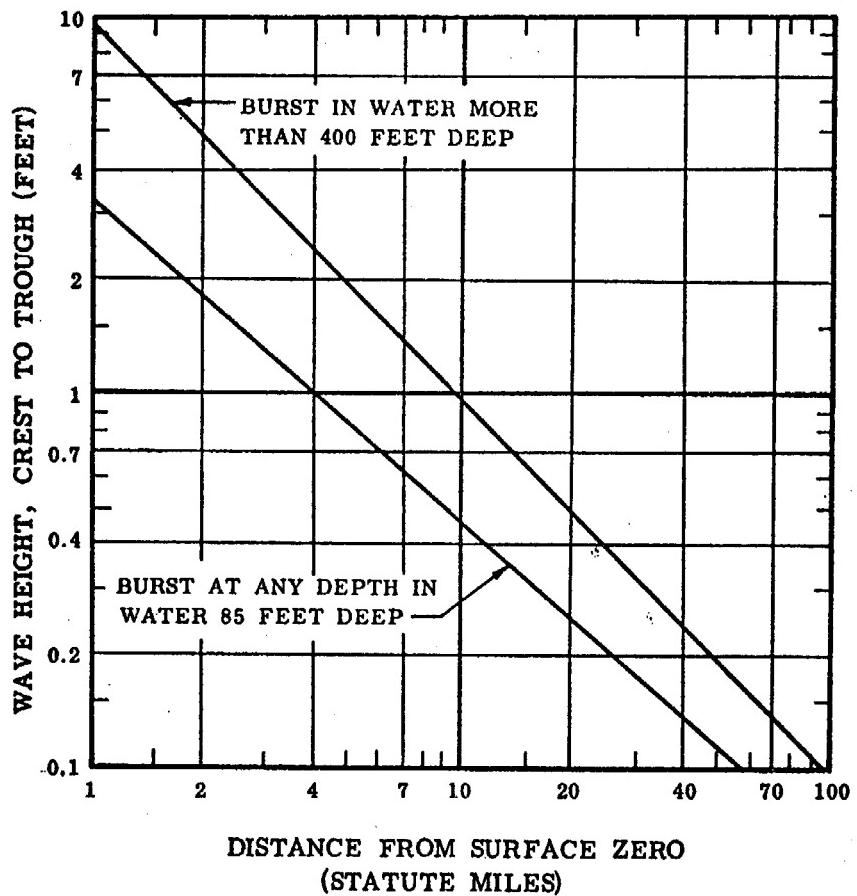


Figure 6.79. Maximum wave height in different types of 1-kiloton underwater bursts.

(from Effects of Nuclear Weapons, 1964, p 311)

SECTION A - BLAST & SHOCK

A-3 TARGET RESPONSE

A-3

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TABLE 4.38a

DAMAGE TO TYPES OF STRUCTURES PRIMARILY AFFECTED BY
BLAST WAVE OVERPRESSURE DURING THE DIFFRACTION
PHASE

Description of structure	Description of damage		
	Severe	Moderate	Light
Multistory reinforced concrete building with reinforced concrete walls, blast resistant design for 30 psi in Mach region from 1 MT; no windows.	Walls shattered, severe frame distortion, incipient collapse.	Walls breached or on the point of being so, frame distorted. Entranceways damaged, doors blown in or jammed, extensive spalling of concrete.	Some cracking of concrete walls and frame.
Multistory reinforced concrete building with concrete walls, small window area; 3 to 8 stories.	Walls shattered, severe frame distortion, incipient collapse.	Exterior walls badly cracked, interior partitions badly cracked or blown down. Structural frame permanently distorted, extensive spalling of concrete.	Windows and doors blown in, interior partitions cracked.
Multistory wall-bearing building, brick apartment house type; up to 8 stories.	Bearing walls collapse, resulting in total collapse of structure.	Exterior walls badly cracked, interior partitions badly cracked or blown down.	Windows and doors blown in, interior partitions cracked.
Multistory wall-bearing building, monumental type; up to 4 stories.	Bearing walls collapse, resulting in collapse of structure supported by these walls; some bearing walls may be shielded enough by intervening walls so that part of the structure may receive only moderate damage.	Exterior walls facing blast badly cracked, interior partitions badly cracked, although toward far end of building damage may be reduced.	Windows and doors blown in, interior partitions cracked.
Wood frame building, house type; 1 or 2 stories.	Frame shattered so that for the most part collapsed.	Wall framing cracked, roof badly damaged, interior partitions blown down.	Windows and doors blown in, interior partitions cracked.

(from Effects of Nuclear Weapons, 1964, p 161)

TABLE 4.38b
DAMAGE TO TYPES OF STRUCTURES PRIMARILY AFFECTED BY
DYNAMIC PRESSURE DURING THE DRAG PHASE

Description of structure	Description of damage		
	Severe	Moderate	Light
Light steel frame industrial building, single story, with up to 5 ton crane capacity. Lightweight, low strength walls fall quickly.	Severe distortion or collapse of frame.	Some to major distortion of frame, cranes (if any) not operable until repairs made.	Windows and doors blown in, light siding ripped off.
Heavy steel frame industrial building, single story, with 25-50 ton crane capacity. Lightweight, low strength walls fall quickly.	Severe distortion or collapse of frame.	Some distortion to frame, cranes not operable until repairs made.	Windows and doors blown in, light siding ripped off.
Heavy steel frame industrial building, single story, with 60-100 ton crane capacity. Lightweight, low strength walls fall quickly.	Severe distortion or collapse of frame.	Some distortion to frame, cranes not operable until repairs made.	Windows and doors blown in, light siding ripped off.
Multistory steel frame office type building, 3-10 stories (earthquake resistant construction). Lightweight, low strength walls fall quickly.	Severe framedistortion, incipient collapse.	Frame distorted moderately, interior partitions blown down.	Windows and doors blown in, light siding ripped off, interior partitions cracked.
Multistory steel frame office type building, 3-10 stories (nonearthquake resistant construction). Lightweight, low strength walls fall quickly.	Severe framedistortion, incipient collapse.	Frame distorted moderately, interior partitions blown down.	Windows and doors blown in, light siding ripped off, interior partitions cracked.
Multistory reinforced concrete frame office type building, 3-10 stories (earthquake resistant construction). Lightweight, low strength walls fall quickly.	Severe framedistortion, incipient collapse.	Frame distorted moderately, interior partitions blown down. Some spalling of concrete.	Windows and doors blown in, light siding ripped off, interior partitions cracked.
Multistory reinforced concrete frame office type building, 3-10 stories (nonearthquake resistant construction). Lightweight, low strength walls fall quickly.	Severe framedistortion, incipient collapse.	Frame distorted moderately, interior partitions blown down. Some spalling of concrete.	Windows and doors blown in, light siding ripped off, interior partitions cracked.
Highway truss bridges, spans 150-250 ft.	Total failure of lateral bracing, collapse of bridge.	Some failure of lateral bracing such that bridge capacity is reduced about 50 percent.	Capacity of bridge unchanged, slight distortion of some bridge components.
Railroad truss bridges, spans 150-250 ft.	Total failure of lateral bracing, collapse of bridge.	Some failure of lateral bracing such that bridge capacity is reduced about 50 percent.	Capacity of bridge unchanged, slight distortion of some bridge components.
Highway and railroad truss bridges, spans 250-500 ft.	Total failure of lateral bracing, collapse of bridge.	Some failure of lateral bracing such that bridge capacity is reduced about 50 percent.	Capacity of bridge unchanged, slight distortion of some bridge components.

(from Effects of Nuclear Weapons, 1964, p 162)

TABLE 4.39
CONDITIONS OF FAILURE OF PEAK OVERPRESSURE-SENSITIVE ELEMENTS

Structural element	Failure	Approximate side-on blast overpressure
Glass windows, large and small.....	Shattering usually, occasional frame failure.....	<i>psi</i> 0.5-1.0
Corrugated asbestos siding.....	Shattering.....	1.0-2.0
Corrugated steel or aluminum paneling.....	Connection failure followed by buckling.....	1.0-2.0
Brick wall panel, 8 in. or 12 in. thick (not reinforced).	Shearing and flexure failures.....	7.0-8.0
Wood siding panels, standard house construction.	Usually failure occurs at the main connections allowing a whole panel to be blown in.	1.0-2.0
Concrete or cinder-block wall panels, 8 in. or 12 in. thick (not reinforced).	Shattering of the wall.....	2.0-3.0

TABLE 4.45
DAMAGE CRITERIA FOR SHALLOW BURIED STRUCTURES

Type of structure	Damage type	Peak over-pressure	Nature of damage
Light, corrugated steel arch, surface structure (10-gage corrugated steel with a span of 20-25 ft), central angle of 180° with 5 ft of earth cover at the crown.*	Severe.....	<i>psi</i> 45-60	Collapse.
	Moderate....	40-50	Large deformations of end walls and arch, also major entrance door damage.
	Light.....	30-40	Damage to ventilation and entrance door.
Buried concrete arch with a 16 ft span and central angle of 180°; 8 in. thick with 4 ft of earth cover at the crown.	Severe.....	220-280	Collapse.
	Moderate....	160-220	Large deformations with considerable cracking and spalling.
	Light.....	120-160	Cracking of panels, possible entrance door damage.

* In the case of arched structures reinforced with ribs, the collapse pressure is higher depending on the number of ribs.

TABLE 4.47
DAMAGE CRITERIA FOR LAND TRANSPORTATION EQUIPMENT

Description of equipment	Damage	Nature of damage
Motor equipment (cars and trucks).	Severe.....	Gross distortion of frame, large displacements, outside appurtenances (door and hoods) torn off, need rebuilding before use.
	Moderate....	Turned over and displaced, badly dented, frames sprung, need major repairs.
	Light.....	Glass broken, dents in body, possibly turned over, immediately usable.
Railroad rolling stock (box, flat, tank, and gondola cars).	Severe.....	Car blown from tracks and badly smashed, extensive distortion, some parts usable.
	Moderate....	Doors demolished, body damaged, frame distorted, could possibly roll to repair shop.
	Light.....	Some door and body damage, car can continue in use.
Railroad locomotives (Diesel or steam).	Severe.....	Overturned, parts blown off, sprung and twisted, major overhaul required.
	Moderate....	Probably overturned, can be towed to repair shop after being righted, need major repairs.
	Light.....	Glass breakage and minor damage to parts, immediately usable.
Construction equipment (bulldozers and graders).	Severe.....	Extensive distortion of frame and crushing of sheet metal, extensive damage to tracks and wheels.
	Moderate....	Some frame distortion, overturning, track and wheel damage.
	Light.....	Slight damage to cabs and housing, glass breakage.

TABLE 4.50
DAMAGE CRITERIA FOR PARKED AIRCRAFT

Damage type	Nature of damage	Overpressure
Severe.....	Major (or depot level) maintenance required to restore aircraft to operational status.	psf
		Transport airplanes..... 3 Light liaison craft..... 2 Helicopters..... 3
Moderate.....	Field maintenance required to restore aircraft to operational status.	Transport airplanes..... 2 Light liaison craft..... 1 Helicopters..... 1.5
Light.....	Flight of the aircraft not prevented, although performance may be restricted.	Transport airplanes..... 1 Light liaison craft..... 0.5 Helicopters..... 0.5

(from Effects of Nuclear Weapons, 1964, pp 166, 167)

TABLE 4.53
DAMAGE CRITERIA FOR SHIPPING FROM AIR BLAST

Damage type	Nature of damage
Severe.....	The ship is either sunk or is damaged to the extent of requiring rebuilding.
Moderate.....	The ship is immobilized and requires extensive repairs, especially to shock-sensitive components or their foundations, e.g., propulsive machinery, boilers, and interior equipment.
Light.....	The ship may still be able to operate, although there will be damage to electronic, electrical, and mechanical equipment.

TABLE 4.55
DAMAGE CRITERIA FOR FORESTS

Damage type	Nature of damage	Equivalent steady wind velocity (miles per hour)
Severe.....	Up to 90 percent of trees blown down; remainder denuded of branches and leaves. (Area impassable to vehicles and very difficult on foot.)	120-140
Moderate.....	About 30 percent of trees blown down; remainder have some branches and leaves blown off. (Area passable to vehicles only after extensive clearing.)	90-100
Light.....	Very few trees blown down; some leaves and branches blown off. (Area passable to vehicles.)	60-80

(from Effects of Nuclear Weapons, 1964, p 169)

TABLE 6.69
DAMAGE CRITERIA FOR MODERATELY DEEP UNDERGROUND
STRUCTURES

Structural type	Damage type	Distance from surface zero	Nature of damage
Relatively small, heavy well-designed underground structures.	Severe.....	1½ apparent crater radii.....	Collapse.
	Light.....	2½ apparent crater radii.....	Slight cracking, severance of brittle external connections.
Relatively long, flexible structures, e.g., buried pipelines, tanks, etc.	Severe.....	1½ apparent crater radii.....	Deformation and rupture.
	Moderate.....	2 apparent crater radii.....	Slight deformation and rupture.
	Light.....	2½ to 3 apparent crater radii.....	Failure of connections.

(from Effects of Nuclear Weapons, 1964, p 300)

Figure 4.58a. Damage-distance relationships for structure of various types.

EXAMPLE 1:

GIVEN: Wood-frame building (Type 1). A 1 MT weapon is burst
 (a) at the optimum height,
 (b) at the surface.

FIND: The ranges from ground zero for severe and moderate damage.

SOLUTION:

(a) From the point 1, at the right, draw a straight line to 1 MT on the severe damage scale and another to 1 MT on the moderate damage scale. The intersections of these lines with the range scale give the required solutions for the optimum burst height, thus,

$$\text{Range for severe damage} = 29,000 \text{ feet}$$

$$\text{Range for moderate damage} = 34,000 \text{ feet} \quad \text{ANSWER}$$

(b) For a surface burst the respective ranges are three-quarters those obtained above; hence,

$$\text{Range for severe damage} = 29,000 \times \frac{3}{4} = 22,000 \text{ feet}$$

$$\text{Range for moderate damage} = 34,000 \times \frac{3}{4} = 26,000 \text{ feet} \quad \text{ANSWER}$$

(The values have been rounded off to two significant figures, since greater precision is not warranted.)

EXAMPLE 2:

GIVEN: A light steel-frame industrial building (Item 8), 2,100 feet from a 10 KT surface burst.

FIND: The nature of the damage to this structure.

SOLUTION:

As this is a surface burst and the data in Fig. 4.58a are for air bursts, the range must be scaled to an air burst equivalent. If surface burst ranges are $\frac{3}{4}$ of air burst ranges, it follows that air burst ranges are $\frac{4}{3}$ of surface burst ranges; hence the scaled distance in this case would be

$$2,100 \times \frac{4}{3} = 2,800 \text{ feet}$$

From point 8, at the right, draw straight lines to 10 KT on the severe damage scale and to 10 KT on the moderate damage scale. Note that 2,800 feet on the range scale lies between these lines. The building is beyond the range of severe damage, but within the range of moderate damage, therefore

Moderate damage

ANSWER

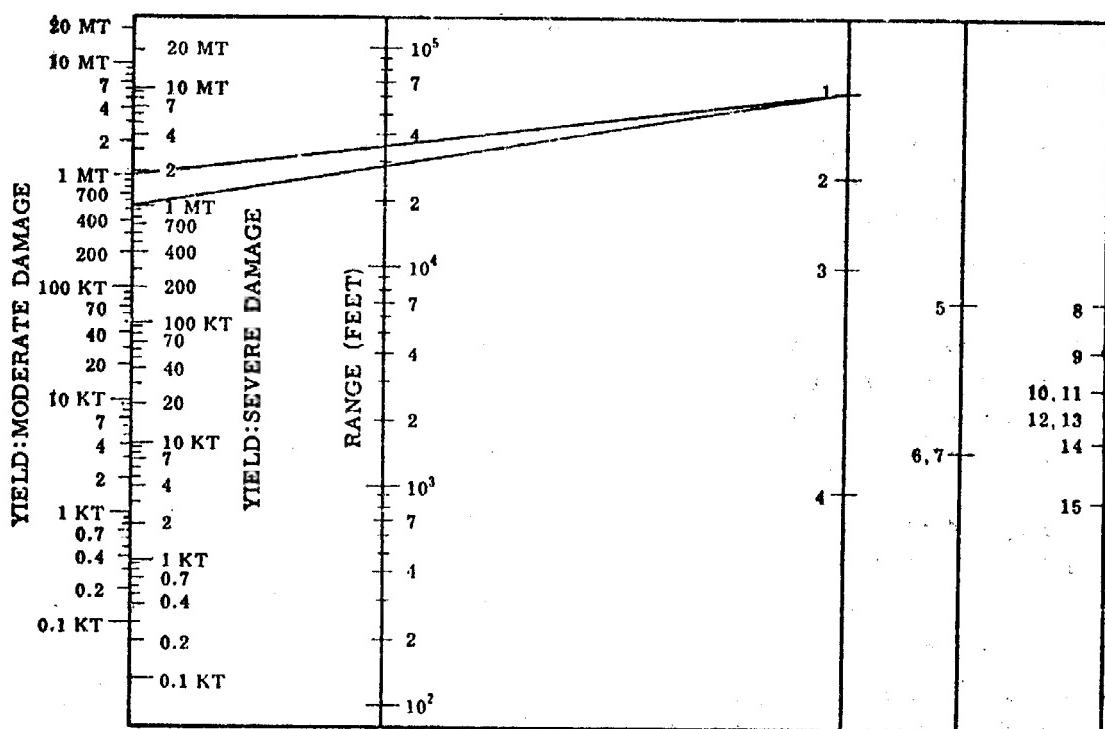


Figure 4.58a. Damage-distance relationships for structures of various types.

TYPES OF STRUCTURES

1. Wood-frame building.
2. Multistory, wall-bearing buildings, brick apartment house type.
3. Multistory, wall-bearing buildings, monumental type.
4. Multistory, blast-resistant design, reinforced-concrete buildings.
5. Multistory, reinforced-concrete buildings, with concrete walls and small window area.
6. Highway truss bridges of 150 to 250 foot span (blast normal to longitudinal bridge axis).
7. Multistory, reinforced-concrete, frame office type buildings, earthquake resistant.
8. Light steel-frame industrial buildings.
9. Heavy steel-frame industrial buildings (25 to 50 ton crane).
10. Heavy steel-frame industrial buildings (60 to 100 ton crane).
11. Railroad truss bridges of 150 to 250 foot span (blast normal to longitudinal bridge axis).
12. Multistory, reinforced-concrete frame office type buildings.
13. Highway and railroad truss bridges of 250 to 400 foot spans (blast normal to longitudinal bridge axis).
14. Multistory, steel-frame office type buildings.
15. Multistory, steel-frame office type buildings, earthquake resistant.

For a surface burst multiply the range by three-quarters.

(from Effects of Nuclear Weapons, 1964, pp 172, 173)

Figure 4.58b. Damage-distance relationships for various targets.EXAMPLE 1:

GIVEN: A transportation type vehicle (Item 3). A 10 KT weapon is burst at
 (a) the optimum height,
 (b) the surface.

FIND: The ranges from ground zero for severe and moderate damage.

SOLUTION:

(a) Draw straight lines from the points z_s and z_m , at the right, to 10 KT on the yield scale at the left. The intersections of these lines with the range scale give the solutions for severe and moderate damage, respectively, for the optimum burst height, thus,

$$\text{Range for severe damage} = 1,900 \text{ feet}$$

$$\text{Range for moderate damage} = 2,900 \text{ feet} \quad \text{ANSWER}$$

(b) For a surface burst the ranges in this case are three-quarters of those obtained above, thus,

$$\text{Range for severe damage} = 1,900 \times \frac{3}{4} = 1,400 \text{ feet}$$

$$\text{Range for moderate damage} = 2,900 \times \frac{3}{4} = 2,200 \text{ feet} \quad \text{ANSWER}$$

EXAMPLE 2:

GIVEN: A motorized scraper (Item 2) located 7,000 feet from a 1 MT surface burst.

FIND: The nature of the damage suffered by this piece of equipment.

SOLUTION:

As this is a surface burst and the data in Fig. 4.58b are for air bursts, the range must be scaled to an air burst equivalent. If surface burst ranges are $\frac{3}{4}$ of air burst ranges, it follows that air burst ranges are $\frac{4}{3}$ of surface burst ranges, hence the scaled distance in this case will be

$$7,000 \times \frac{4}{3} = 9,300 \text{ feet} \quad (2 \text{ figs.})$$

Draw a straight line from 1 MT on the yield scale, on the left, through 9,300 feet (9.3×10^3) on the range scale to the extreme right hand scale. Note that it intersects the right hand scale between 2_m and 2_s .

The scraper is beyond the range of severe damage (2_s), but within the range of moderate damage, therefore

Moderate damage

ANSWER

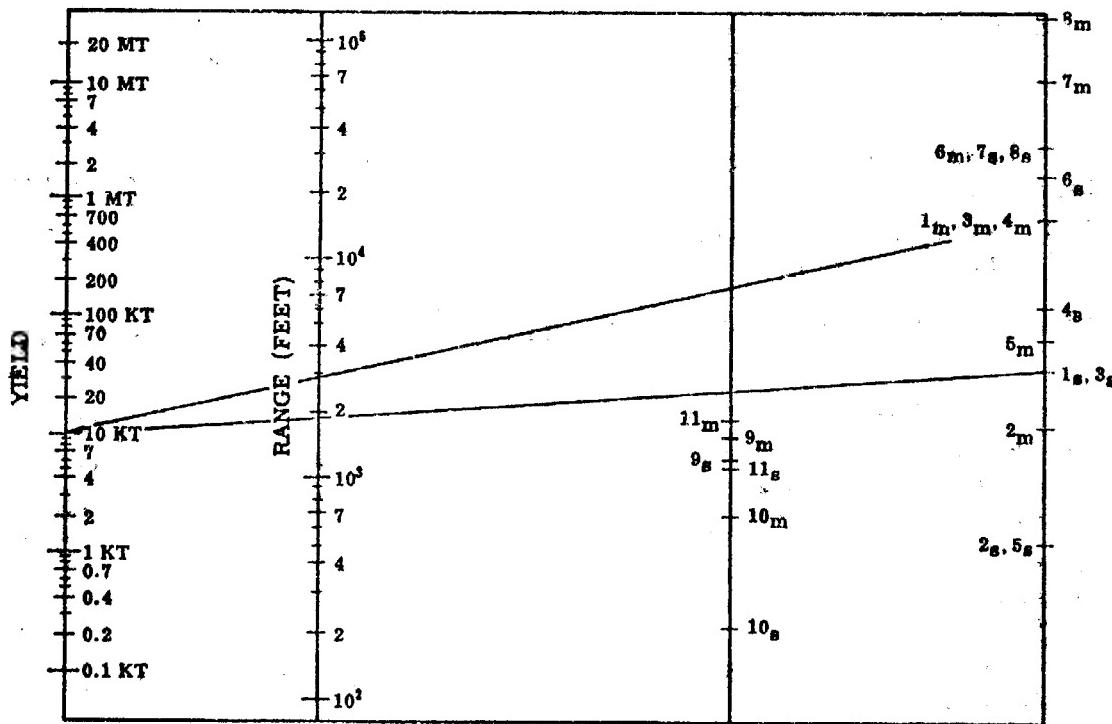


Figure 4.58b. Damage-distance relationships for various targets.

TARGETS

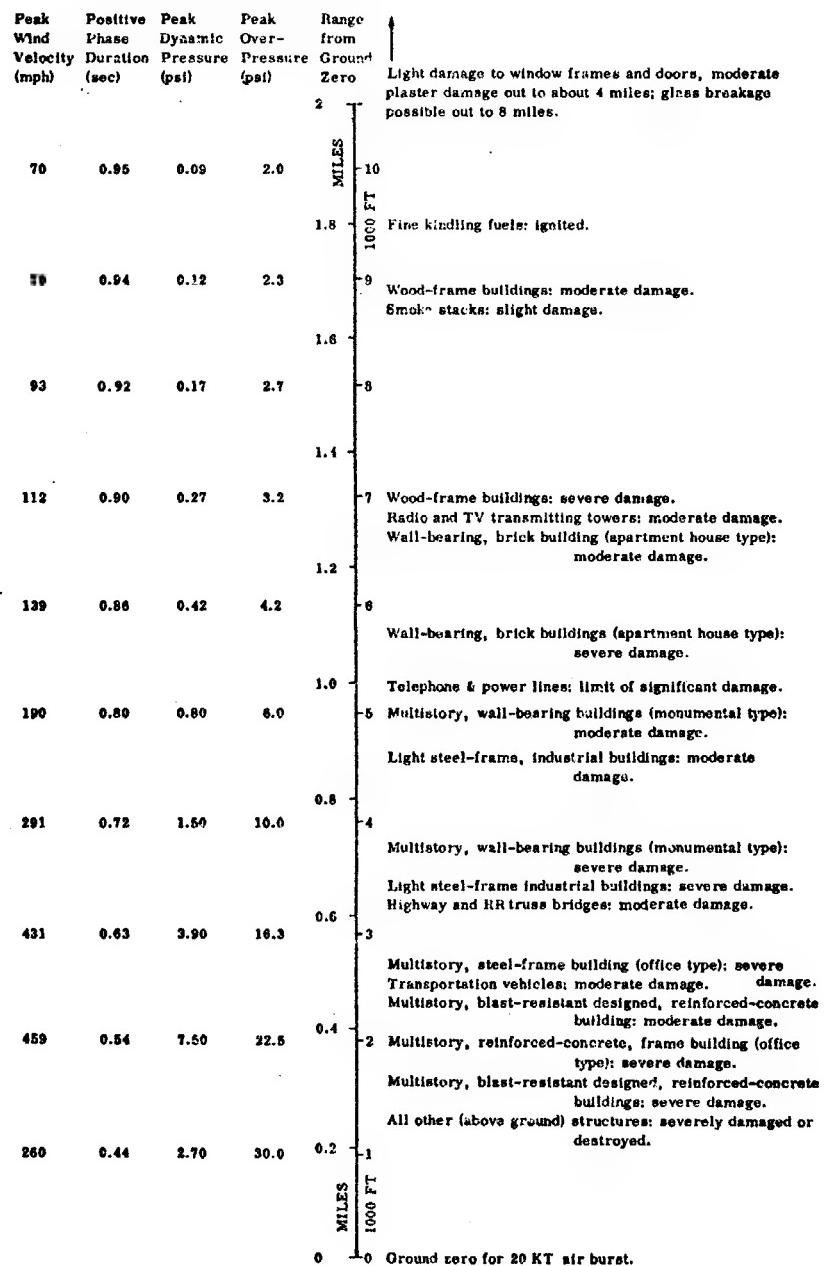
1. Truck mounted engineering equipment (unprotected).
2. Earth moving engineering equipment (unprotected).
3. Transportation vehicles.
4. Boxcars, flatcars, full tank cars, and gondola cars (side-on orientation).
5. Locomotives (side-on orientation).
6. Telephone lines (radial).
7. Telephone lines (transverse).
8. Average forest stand.
9. Boxcars, flatcars, full tank cars, and gondola cars (end-on orientation).
10. Locomotives (end-on orientation).
11. Merchant shipping.

Subscript "m" refers to moderate damage and subscript "s" refers to severe damage.

For a surface burst multiply the range by three-quarters for Items 1 through 8. For Items 9, 10, and 11, the ranges are the same for a surface burst as for the optimum burst height.

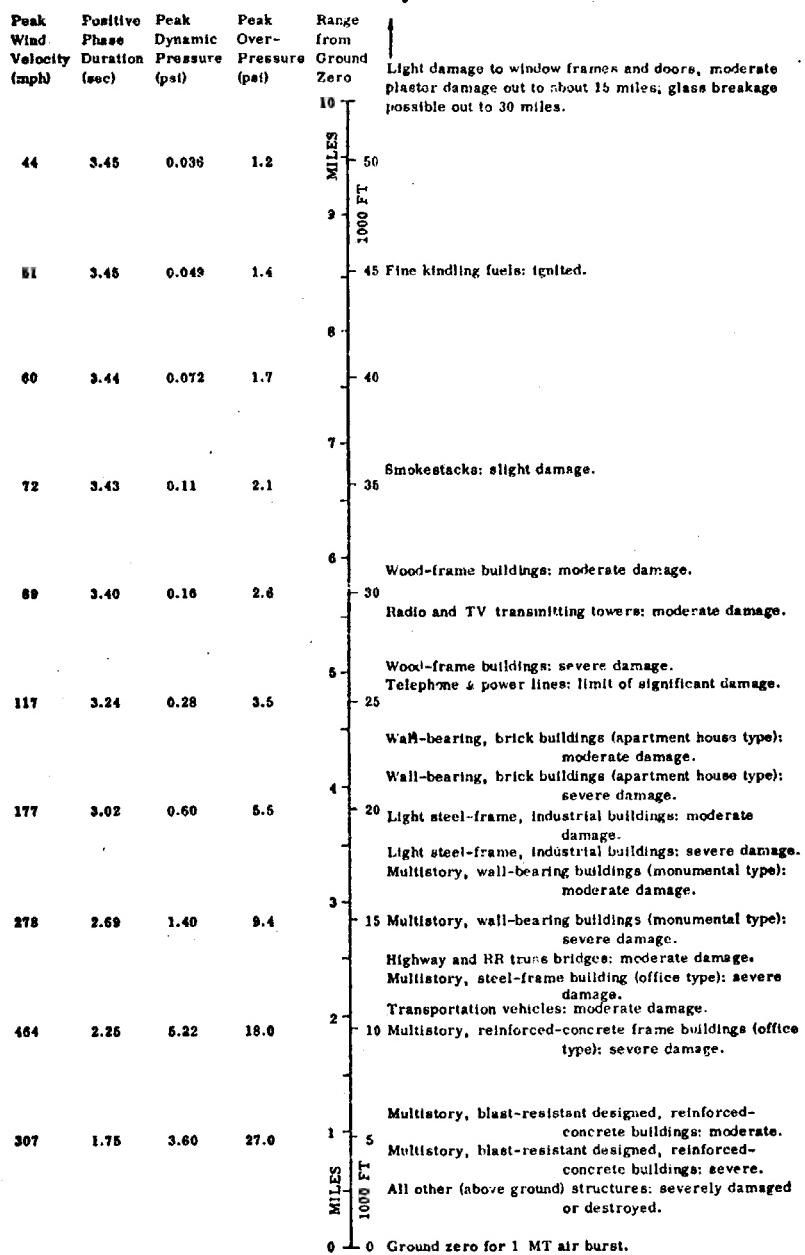
(from Effects of Nuclear Weapons, 1964, pp 174, 175)

TABLE 12.22a
DAMAGE RANGES FOR 20-KT TYPICAL AIR BURST



(from Effects of Nuclear Weapons, 1964, p 639)

TABLE 12.22b
DAMAGE RANGES FOR 1-MT TYPICAL AIR BURST



(from Effects of Nuclear Weapons, 1964, p 640)

SECTION B - THERMAL RADIATION & EFFECTS

B-1 EMISSION, TRANSMISSION & DELIVERY

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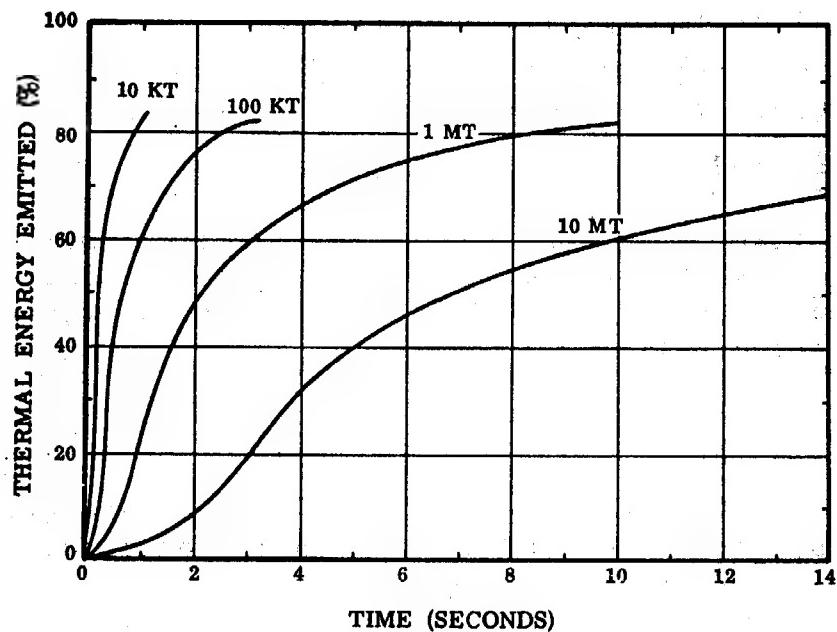


Figure 7.95. Percentage of thermal energy emitted as a function of time for air bursts of various yields.

(from Effects of Nuclear Weapons, 1964, p 360)

Figure 7.91. Scaled fireball power and fraction of thermal energy versus scaled time in second thermal pulse of an air burst.

The curves in Fig. 7.91 show the variation with the scaled time, t/t_{max} , of the scaled fireball power, P/P_{max} (left ordinate) and of the percent of the total thermal energy emitted, E/E_{tot} (right ordinate), in the second thermal pulse of an air burst.

SCALING:

In order to apply the data in Fig. 7.91 to an explosion of any energy, W kilotons, the following expressions are used:

$$P_{max} \quad 4W^{\frac{1}{2}} \text{ kilotons per second}$$

$$t_{max} \quad 0.032 W^{\frac{1}{2}} \text{ seconds}$$

$$E_{tot} \quad \frac{1}{3}W \text{ kilotons,}$$

Where t_{max} is the time after explosion for temperature maximum in second thermal pulse, P_{max} is the maximum rate (at t_{max}) of emission of thermal energy from fireball, and E_{tot} is the total thermal energy emitted by fireball in the second pulse.

EXAMPLE:

GIVEN: A 500 KT burst

FIND: (a) The rate of emission of thermal energy,
 (b) The amount of thermal energy emitted, at 2 seconds
 after the explosion.

SOLUTION:

Since W is 500 KT, the value of $W^{\frac{1}{2}}$ is 22.4, so that $t_{max} = 0.032 \times 22.4 = 0.72$ second, and the scaled time at 2 seconds after the explosion is

$$t/t_{max} = \frac{2.0}{0.72} = 2.8$$

(a) From Fig. 7.91, the value of P/P_{max} at this scaled time is 0.26, and since $P_{max} = 4 \times 22.4 = 90$ kilotons per second, it follows that,

$$\begin{aligned} P &= 0.26 \times 90 = 23 \text{ kilotons per second} \\ &= 23 \times 10^{12} \text{ calories per second} \quad \text{ANSWER} \end{aligned}$$

(b) At the scaled time of 2.8, the value of E/E_{tot} from Fig. 7.91 is 58 percent, i.e., 0.58, and

$$E_{tot} = 1/3 \times 500 = 167 \text{ kilotons}$$

Hence,

$$E = 0.58 \times 167 = 97 \text{ kilotons}$$

$$= 97 \times 10^{12} \text{ calories} \quad \text{ANSWER}$$

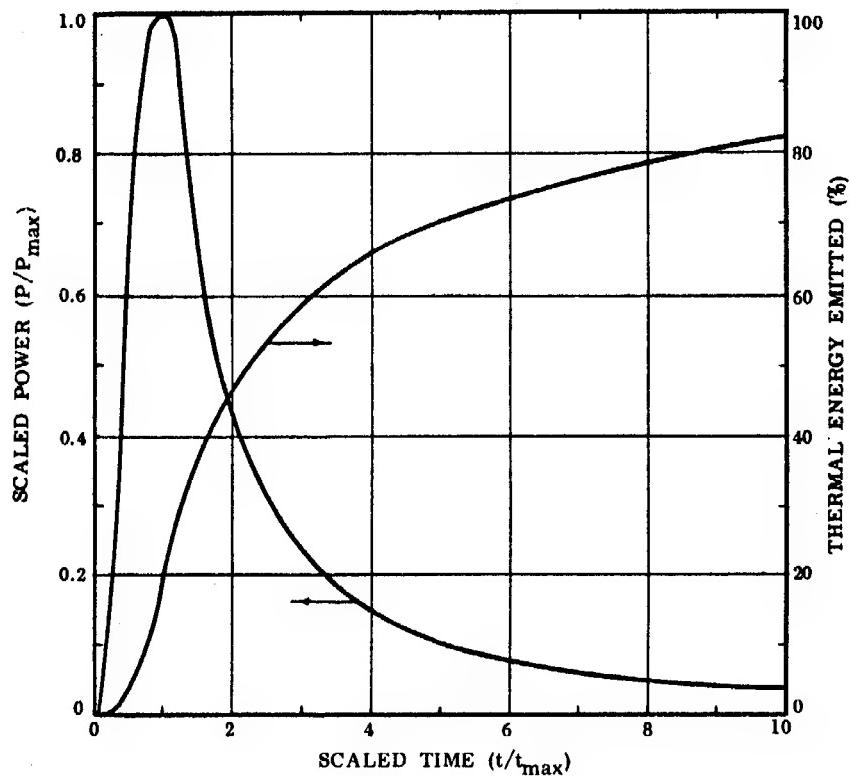


Figure 7.01. Scaled fireball power and fraction of thermal energy versus scaled time in second thermal pulse of an air burst.

(from Effects of Nuclear Weapons, 1964, p 359)

LAND SURFACE	HEIGHT OF BURST in FEET	VISIBILITY in MILES	TRANSMISSION COEFFICIENTS τ_A								
			0	10,000	20,000	30,000	40,000	50,000	60,000	70,000	80,000
Bare of snow	5,000	2	0.53	0.20	0.05	0.01					
Bare of snow	30,000	2	0.19	0.16	0.13	0.10	0.07	0.05	0.04	0.02	
Bare of snow	5,000	10	0.90	0.75	0.50	0.32	0.23	0.16	0.10	0.08	0.06
Bare of snow	30,000	10	0.64	0.58	0.54	0.48	0.44	0.38	0.34	0.29	
Snow covered	5,000	10	1.05	1.12	0.80	0.50	0.30	0.20	0.15	0.10	0.06
Snow covered	30,000	10	0.58	0.56	0.51	0.47	0.43	0.37	0.33	0.30	
Snow covered	5,000	50	1.05	1.40	1.40	1.25	1.06	0.92	0.78	0.68	0.63
Snow covered	30,000	50	0.78	0.73	0.68	0.63	0.60	0.57	0.54	0.52	0.49
Bare of snow	0	2	0.58	0.13	0.02	0.01					
Bare of snow	0	10	0.90	0.64	0.35	0.19	0.11	0.07	0.04		
Snow Covered	0	50	1.0	0.90	0.75	0.63	0.54	0.47	0.42	0.38	

Table 4.10.1 TRANSMISSION COEFFICIENTS, τ_A , FOR VARIOUS ATMOSPHERIC AND GROUND COVER CONDITIONS

(from Incendiary Effects of Nuclear Weapons, Canada EMO, 1964, p 16)

GLAZING AND WINDOW SCREEN COMBINATIONS	TRANSMISSION COEFFICIENT τ_w
None	1.00
Single Window Screen	0.67
Single Pane Glazing	0.56
Single Pane Glazing, Single Screen	0.37
Double Pane Glazing	0.31
Double Pane Glazing, Single Screen	0.21

Table 5.11.1 TRANSMISSION COEFFICIENT, τ_w ,
FOR RADIANT HEAT THROUGH WINDOW GLASS AND MESH SCREEN²

(from Incendiary Effects of Nuclear Weapons, Canada EMO, 1964, p 32)

B - 1

EMISSION, TRANSMISSION & DELIVERY

THERMAL

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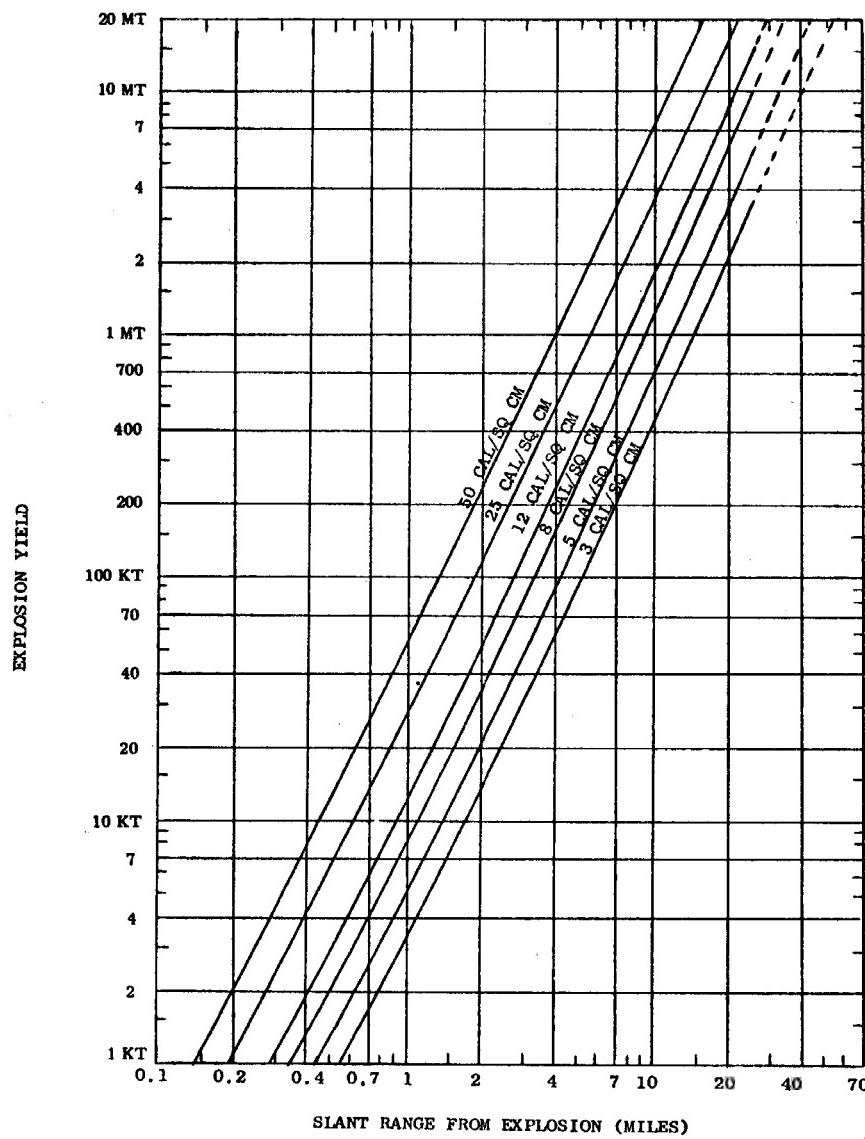


Figure 7.47. Slant ranges for specified radiant exposures as a function of energy yield of an explosion at moderate altitude (less than 20 miles) for 50-mile visibility.

(From Effects of Nuclear Weapons, 1964, p 333)

Figure 7.105. Radiant exposure as a function of slant range from a 1-kiloton air burst for visibilities of 10 miles and 50 miles.

The plot in Fig. 7.105, which is in two parts for convenience of representation, shows the amount of thermal energy (or radiant exposure) in calories per square centimeter received at various distances from a 1 KT air burst for atmospheric visibility between 10 and 50 miles.

SCALING:

The radiant exposure at any specified distance from a W KT explosion is W times the value for the same distance from a 1 KT burst.

EXAMPLE:

GIVEN: A 100 KT air burst and a visibility of between 10 and 50 miles.

FIND: The radiant exposure received at a distance of 3 miles from the explosion.

SOLUTION:

From Fig. 7.105 the amount of thermal energy received at 3 miles from a 1 KT air burst is between 0.07 and 0.10 calorie per square centimeter. Consequently, the radiant exposure received at 3 miles from a 100 KT air burst is between

$$100 \times 0.07 = 7 \text{ calories per square centimeter}$$

and

$$100 \times 0.10 = 10 \text{ calories per square centimeter} \quad \text{ANSWER}$$

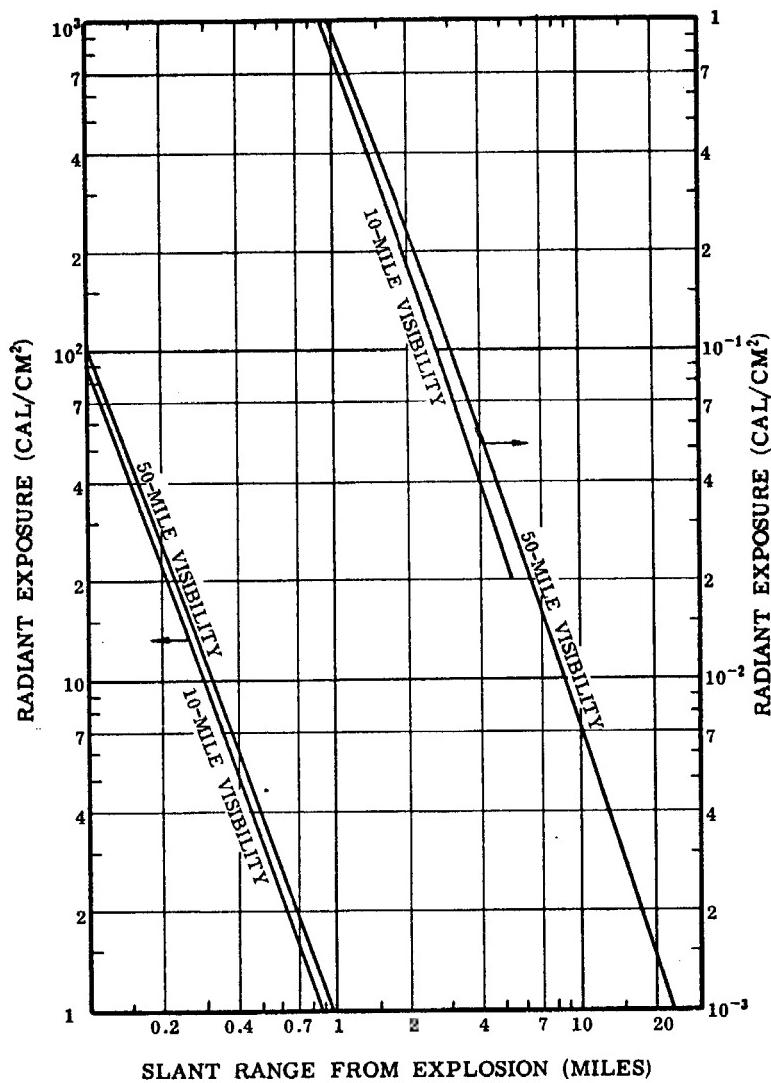


Figure 7.105. Radiant exposure as a function of slant range from a 1-kiloton air burst for visibilities of 10 miles and 50 miles.

(from Effects of Nuclear Weapons, 1964, p 365)

SECTION B - THERMAL RADIATION & EFFECTS

B-2 IGNITION & SPREAD OF FIRES

B-2

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TABLE 7.40
APPROXIMATE RADIANT EXPOSURES FOR IGNITION OF FABRICS*

Material	Weight	Ignition exposure** (cal/sq cm)			
		oz/sq yd	40 kilotons	1 megaton	10 megatons
Rayon gabardine (black).....	6		9	20	26
Rayon-acetate drapery (wine).....	5		9	22	28
Rayon gabardine (gold) #.....	7	(***)	24		28
Rayon twill lining (black).....	8	7	17	25	
Rayon twill lining (beige).....	8	13	20	28	
Acetate-shantung (black) #.....	8	10	22	35	
Cotton chenille bedspread (light blue) #.....		(***)	11	18	
Cotton venetian blind tape, dirty (white).....		10	18	22	
Cotton muslin oiled window shade (green).....	8	7	13	19	
Cotton corduroy (brown).....	8	11	16	22	
Cotton canvas (O.D.).....	12	12	18	28	
Cotton denim, new (blue).....	10	12	27	44	
Cotton venetian blind strap (white) #.....		18	27	31	
Cotton shirting (khaki).....	8	14	21	28	
Cotton heavy draperies (dark colors).....	18	15	18	34	

*Certain materials listed in previous editions and printings have been deleted.

**The values given are for near sea level detonations of weapons of the yields indicated. Ignition levels (except where marked #) are estimated to be valid within $\pm 25\%$ under standard laboratory conditions. Under typical field conditions the values listed are estimated to be valid within $\pm 50\%$ with a greater likelihood of higher rather than lower values. For materials marked #, ignition levels are estimated to be valid within $\pm 50\%$ under laboratory conditions and within $\pm 100\%$ under field conditions.

***Data not available or appropriate scaling not known.

TABLE 7.44
APPROXIMATE RADIANT EXPOSURE FOR IGNITION OF HOUSEHOLD MATERIALS AND DRY FOREST FUELS*

Material	Weight	Ignition exposure** (cal/sq cm)			
		oz/sq yd	40 kilotons	1 megaton	10 megatons
Newspaper, shredded.....	2		4	6	11
Newspaper, dark picture area.....	2		5	7	12
Newspaper, printed text area.....	2		6	8	15
Paper, crepe (green).....	1		6	9	16
Cotton string scrubbing mop, used (gray) #.....		10	15	21	
Cotton string mop, weathered (cream) #.....		10	19	26	
Matches, paper book, blue head exposed #.....		11	14	20	
Excelsior, ponderosa pine (light yellow) #.....	2 lb/cu ft	(***)	23	23	
Paper, Kraft, single sheet (tan).....	3	10	13	20	
Paper, bristol board, 3 ply (dark).....	10	16	20	40	
Paper, Kraft, carton, flat side, used (brown).....	16	16	20	40	
Paper, bond, typing, new (white) #.....	2	24	30	50	
Dry rotted wood punk (fir) #.....		4	6	8	
Deciduous leaves (beech).....		4	6	8	
Fine grass (cheat).....		5	8	10	
Coarse grass (sedge).....		6	9	11	
Pine needles, brown (ponderosa).....		10	16	21	

*Certain materials listed in previous editions and printings have been deleted.

**The values given are for near sea level detonations of weapons of the yields indicated. Ignition levels (except where marked #) are estimated to be valid within $\pm 25\%$ under standard laboratory conditions. Under typical field conditions the values listed are estimated to be valid within $\pm 50\%$ with a greater likelihood of higher rather than lower values. For materials marked #, ignition levels are estimated to be valid within $\pm 50\%$ under laboratory conditions and within $\pm 100\%$ under field conditions.

***Data not available or appropriate scaling not known.

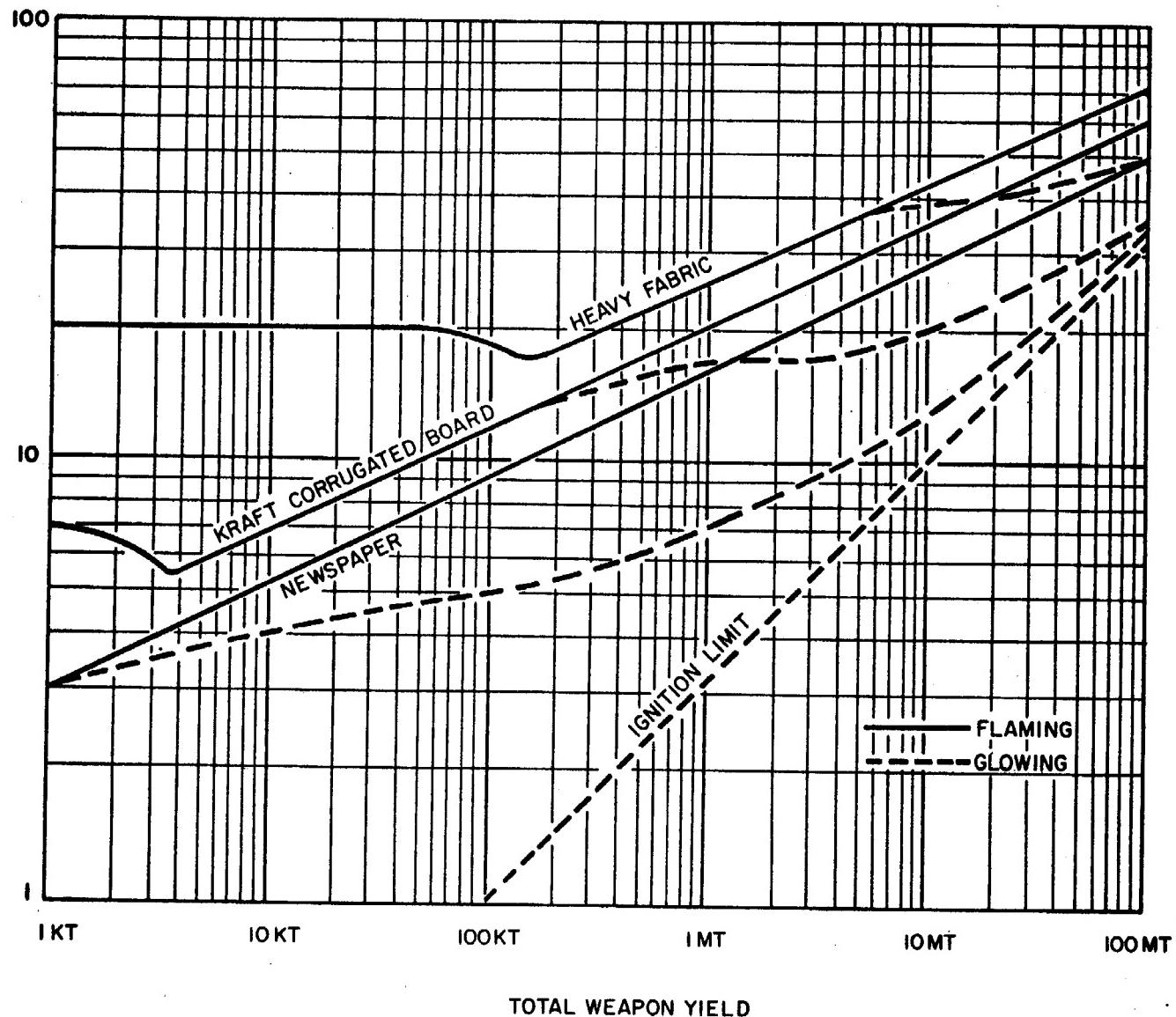
RADIANT EXPOSURES FOR IGNITION IN CAL.CM.⁻²

FIG. 7.16.I RADIANT EXPOSURES TO IGNITE MATERIALS (40 TO 50% RELATIVE HUMIDITY) AS A FUNCTION OF TOTAL WEAPON YIELD, TAKEN FROM "THERMAL RADIATION AND FIRE EFFECTS OF NUCLEAR DETONATIONS" BY S.MARTIN AND A.BROIDO^⑨

(from Incendiary Effects of Nuclear Weapons, Canada EMO, 1964, p 45)

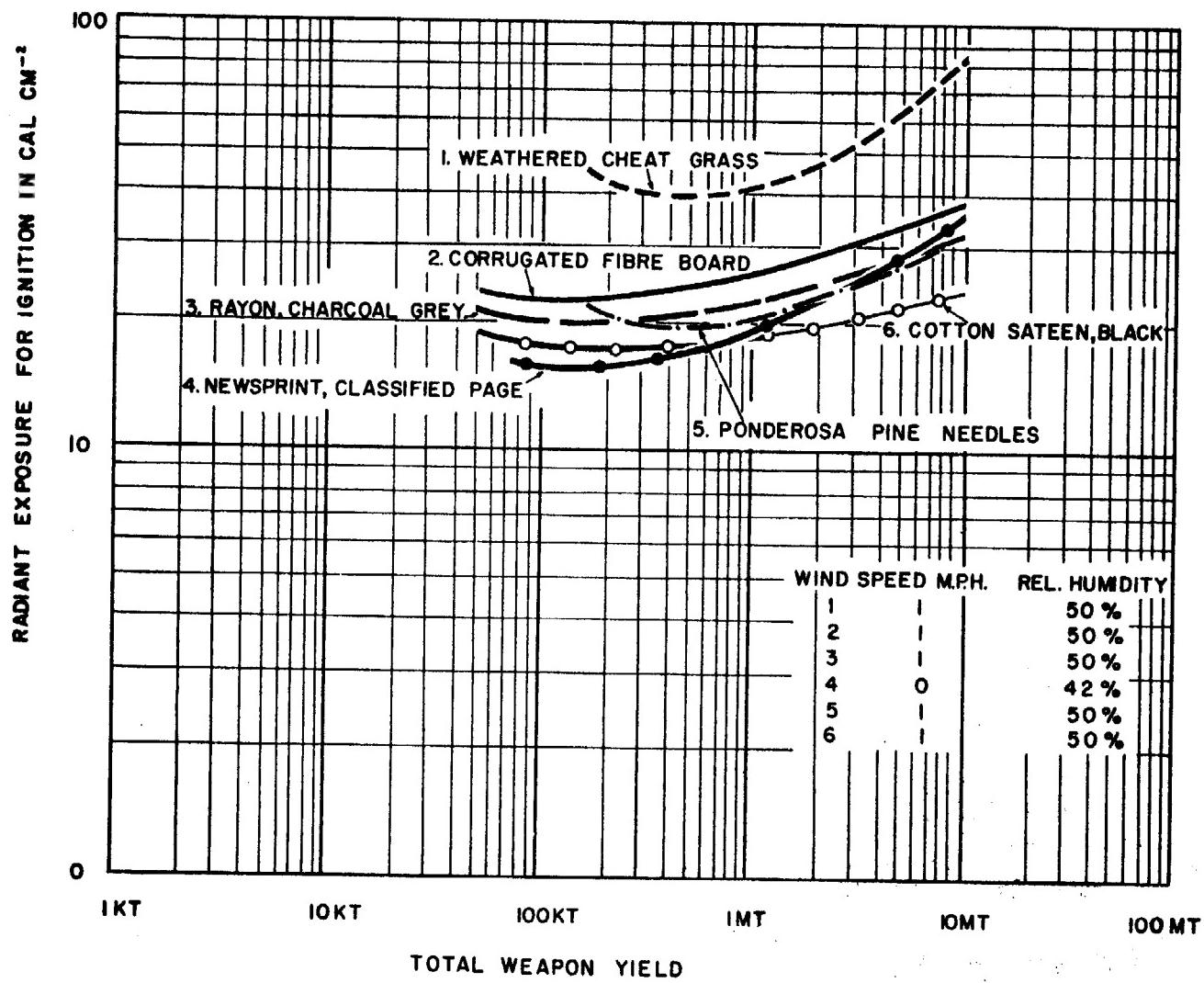


FIG. 7.16.2 RADIANT EXPOSURES TO IGNITE VARIOUS MATERIALS AS A FUNCTION OF TOTAL WEAPON YIELD, TAKEN FROM "TECHNICAL OBJECTIVE AW-7" by J. BRACCIAVENTI & F. DEBOLD, JULY 1960.

(from Incendiary Effects of Nuclear Weapons, Canada EMO, 1964, p 46)

			MAXIMUM DISTANCE FROM GROUND ZERO AT WHICH NEWSPAPER MAY SUSTAIN SPONTANEOUS FLAMING IGNITION. (FEET). TOTAL ENERGY YIELD OF WEAPON = 5 MEGATONS						
LAND SURFACE	HEIGHT OF BURST in Feet	VISIBILITY in Miles	GLAZING AND WINDOW SCREEN COMBINATIONS						PRIMARY IGNITION
			NONE	SINGLE WINDOW SCREEN	SINGLE PANE GLAZING	SINGLE PANE GLAZING SINGLE SCREEN	DOUBLE PANE GLAZING	DOUBLE PANE GLAZING SINGLE SCREEN	
Bare of Snow	5,000	2	21,000	17,000	16,500	14,500	14,000	12,000	Probable
			23,500	21,000	20,000	19,500	19,000	17,000	Possible
Bare of Snow	30,000	2	0	0	0	0	0	0	Probable
			28,000	21,000	18,000	8,000	2,000	0	Possible
Bare of Snow	5,000	10	36,000	31,000	30,000	25,500	24,500	21,500	Probable
			50,000	45,000	43,000	38,000	36,000	31,500	Possible
Bare of Snow	30,000	10	36,000	26,500	23,000	11,000	4,500	0	Probable
			64,000	53,000	50,000	40,000	36,500	27,000	Possible
Snow Covered	5,000	10	39,000	35,000	33,500	30,000	28,000	25,000	Probable
			54,000	48,000	46,000	41,000	39,000	35,500	Possible
Snow Covered	30,000	10	35,000	26,000	21,500	10,000	0	0	Probable
			64,000	53,500	49,000	40,000	36,000	26,500	Possible
Snow Covered	5,000	50	61,000	53,000	50,000	42,000	40,000	34,000	Probable
			90,000±	80,000	76,000	65,000	61,000	54,000	Possible
Snow Covered	30,000	50	44,000	33,000	28,500	18,000	13,000	0	Probable
			82,000	68,000	62,000	49,000	45,000	34,000	Possible
Bare of Snow	0	2	16,500	15,000	14,500	13,000	12,500	11,000	Probable
			19,500	19,000	18,000	17,500	17,000	15,500	Possible
Bare of Snow	0	10	30,000	27,000	26,000	23,000	22,000	19,500	Probable
			41,000	37,500	36,000	32,000	30,000	27,500	Possible
Snow Covered	0	50	48,000	41,000	39,000	33,000	30,000	26,000	Probable
			75,000±	65,000	61,000	52,000	48,500	42,000	Possible

Figure 7.22.1 DISTANCE FROM GROUND ZERO OF A 5 MEGATON TOTAL ENERGY YIELD NUCLEAR WEAPON AT WHICH SPONTANEOUS SUSTAINED FLAMING IGNITION OF NEWSPAPER MAY RESULT UNDER VARYING CONDITIONS OF ALTITUDE OF DETONATION, LAND SURFACE COVER, VISIBILITY AND WINDOW GLAZING AND SCREENING.

(from Incendiary Effects of Nuclear Weapons, Canada EMO, 1964, p 52)

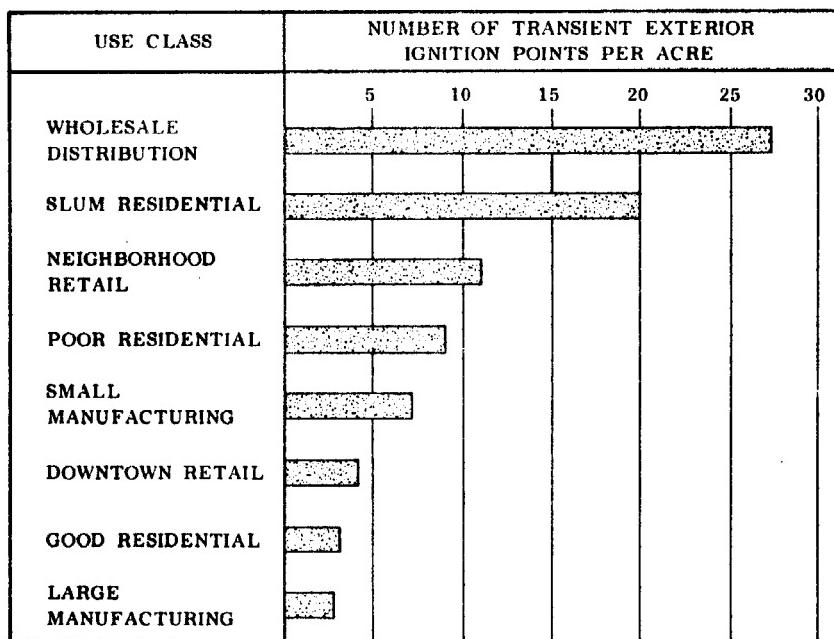


Figure 7.55. Frequency of exterior ignition points for various areas in a city

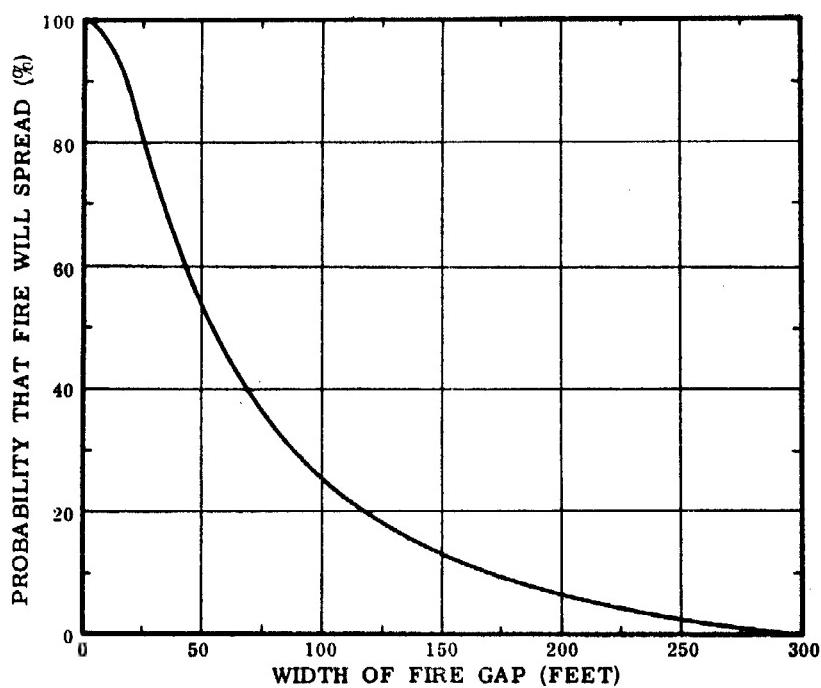


Figure 7.62. Width of gap and probability of fire spread.

(from Effects of Nuclear Weapons, 1964, pp 341, 344)

SECTION B - THERMAL RADIATION & EFFECTS

B - 3 SKIN BURNS

B-3

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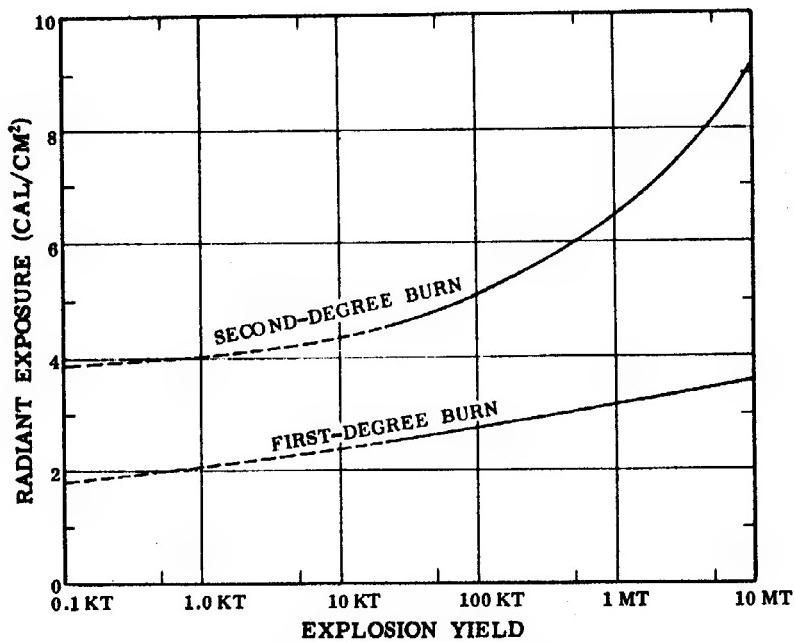


Figure 11.61. Radiant exposures required to produce first- and second-degree burns as a function of total energy yield.

(from Effects of Nuclear Weapons, 1964, p 571)

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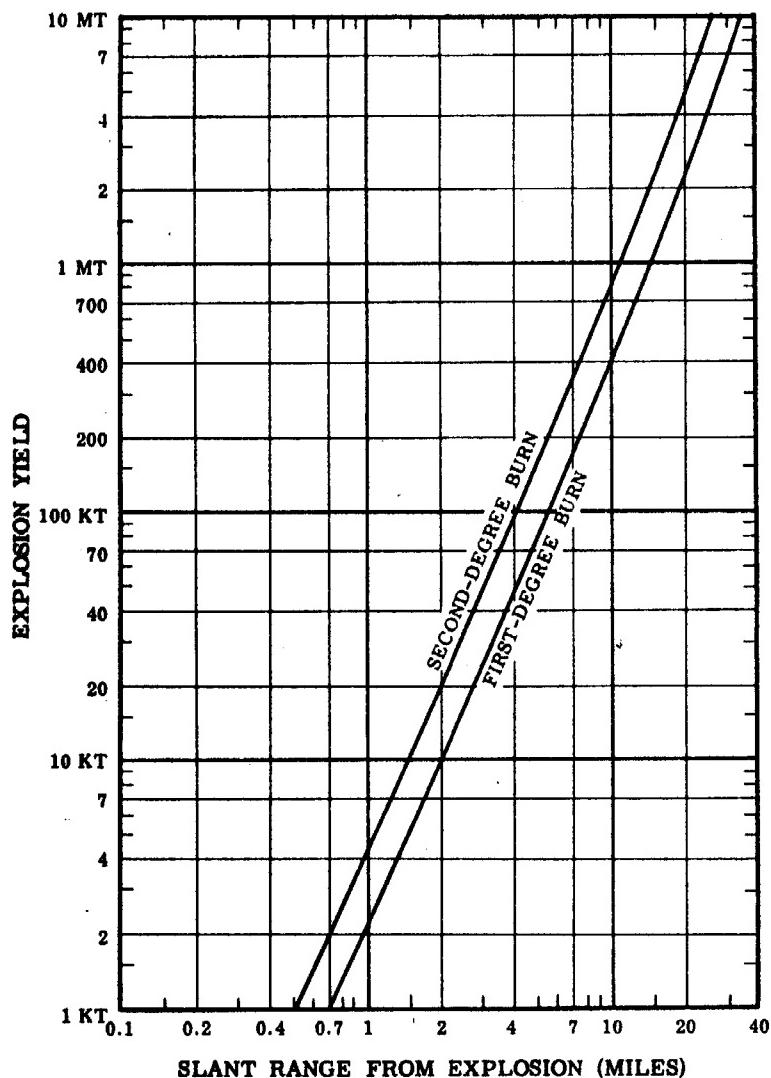


Figure 11.63. Ranges for first- and second-degree burns as a function of the total energy yield.

(from Effects of Nuclear Weapons, 1964, p 573)

SECTION C - INITIAL NUCLEAR RADIATION

C-1 GAMMA

C-1

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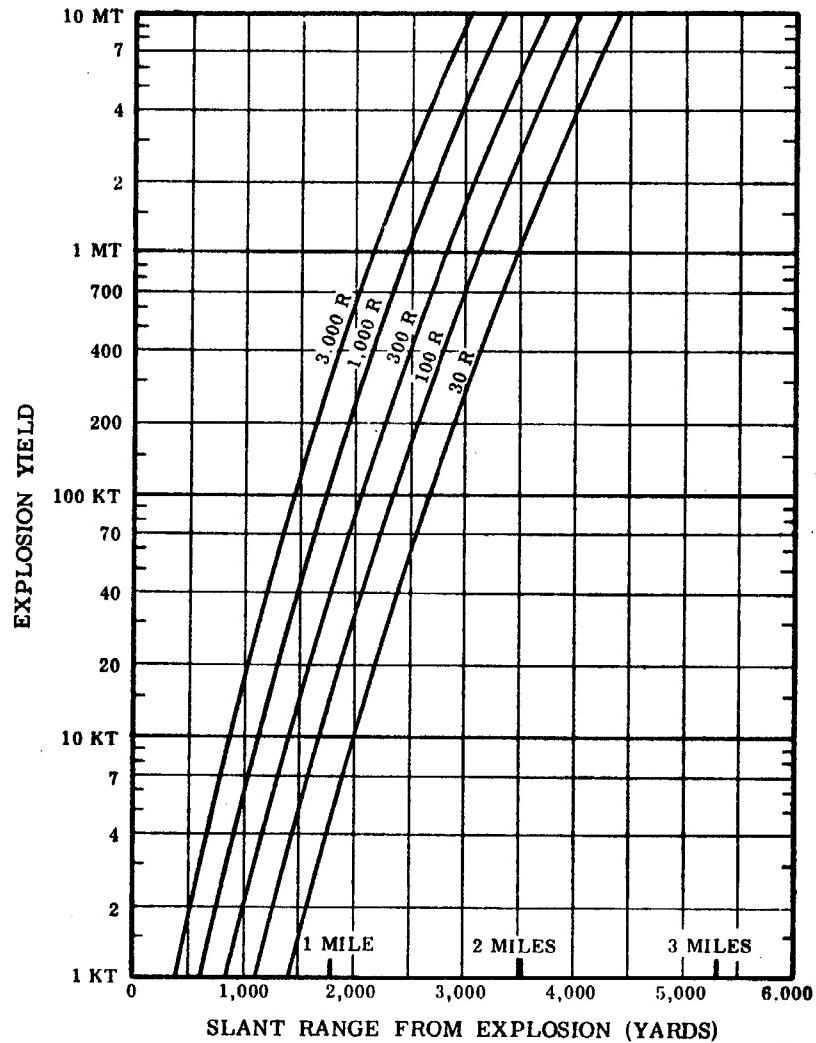


Figure 8.31. Slant ranges for specified initial gamma-ray doses as function of energy yield of the explosion.

(from Effects of Nuclear Weapons, 1964, p 380)

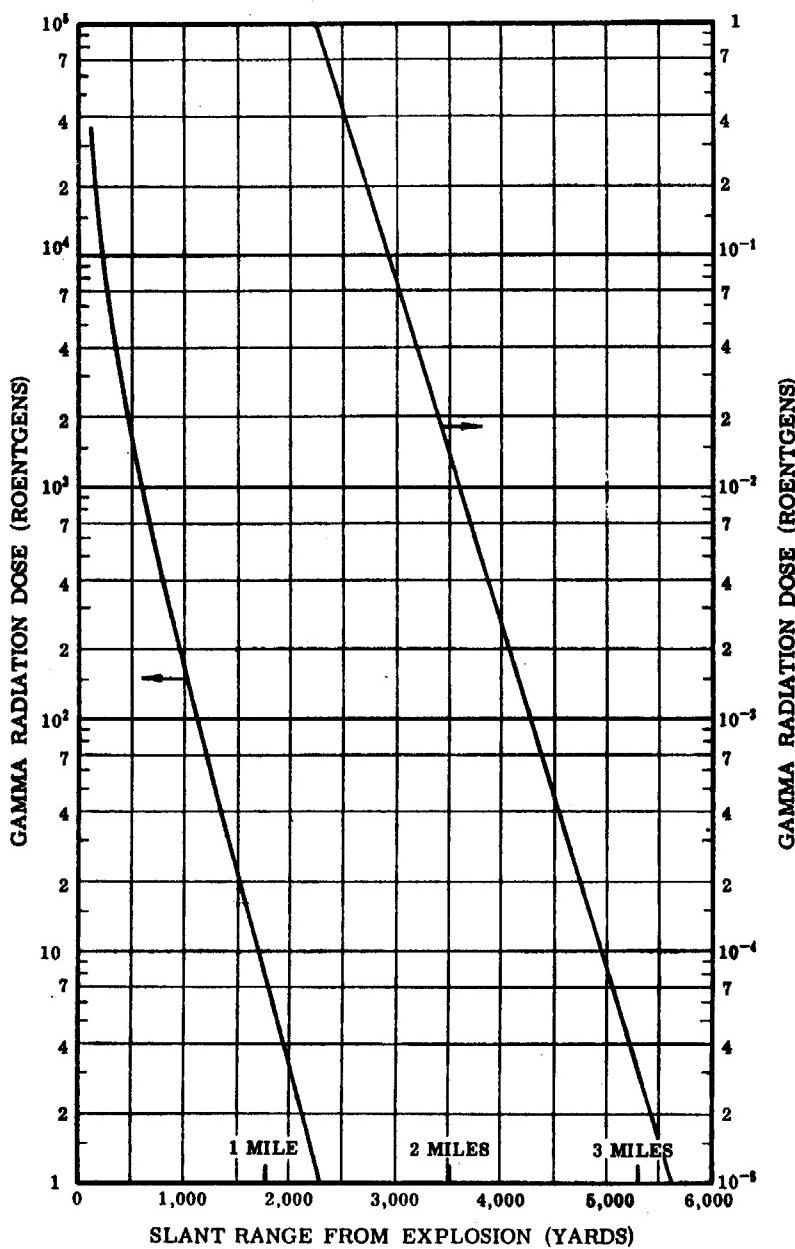


Figure 8.27a. Initial gamma-radiation dose as function of slant range from explosion for 1-kiloton air burst, based on 0.9 sea-level air density.

(from Effects of Nuclear Weapons, 1964, p 377)

The gamma-radiation exposure doses at known distances from explosions of different energy yields have been measured at a number of nuclear test explosions. The results obtained from air bursts are summarized in the form of two graphs: the first (Fig. 8.27a) shows the dependence of the initial gamma-ray dose on the actual distance (slant range) from a 1-kiloton explosion; the second (Fig. 8.27b) gives the

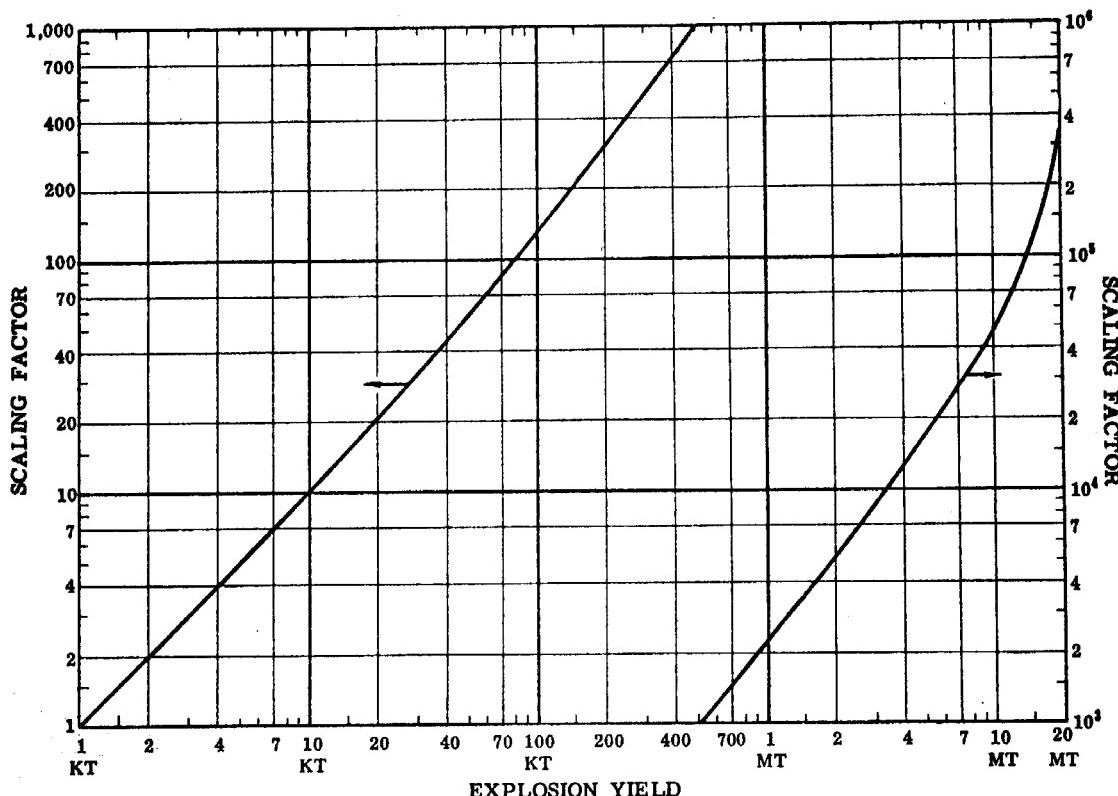


Figure 8.27b. Scaling factor for initial gamma-radiation dose.

(from Effects of Nuclear Weapons, 1964, p 378)

scaling factor to be used to determine the dose at the same slant range from an explosion of any specific energy yield up to 20 megatons*.

EXAMPLE:

GIVEN: 100-kiloton air burst.

FIND: Initial gamma-radiation dose at a distance of 1,700 yards.

SOLUTION:

From Fig. 8.27a, the exposure dose at this distance from a 1 KT air burst is 10 roentgens.

From Fig. 8.27b, the scaling factor for 100 KT is 120.

Hence, the gamma dose in this case is

$$10 \times 120 = 1,200 \text{ roentgens}$$

ANSWER

* See ENW, para. 8.27 and footnote.

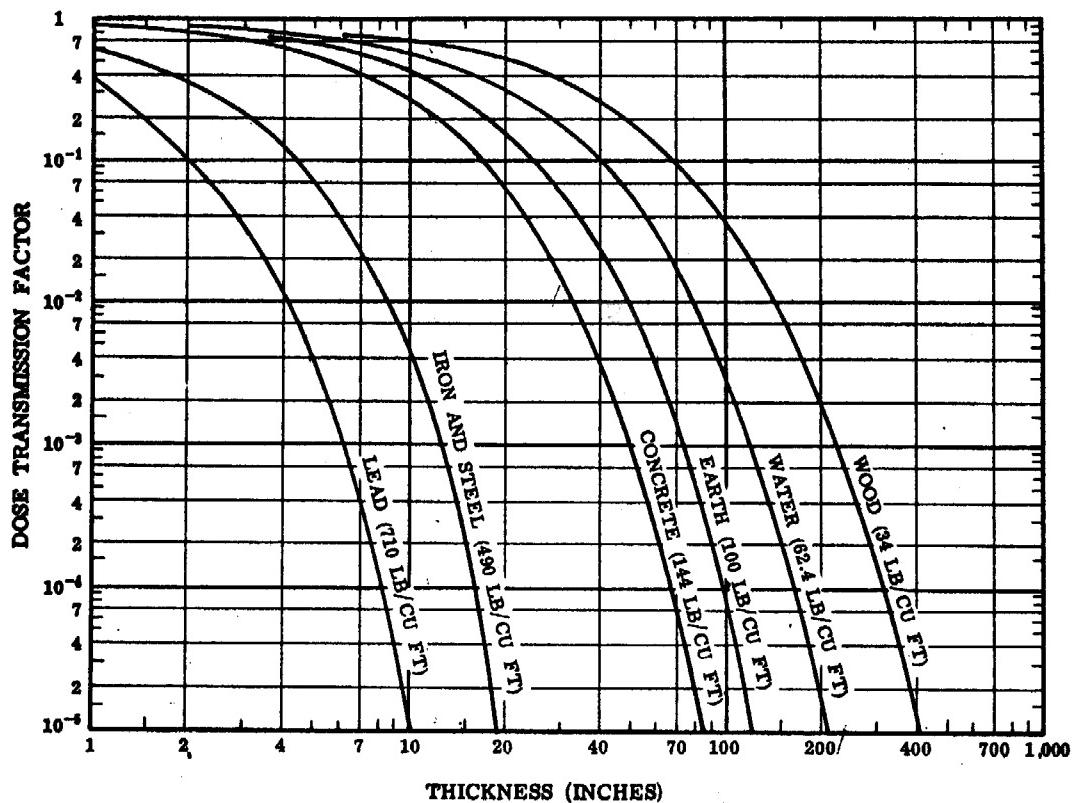


Figure 8.38. Dose transmission factors for initial gamma radiations of various materials as function of thickness.

(from Effects of Nuclear Weapons, 1964, p 384)

SECTION C - INITIAL NUCLEAR RADIATION

C-2 COMBINED NEUTRON & GAMMA

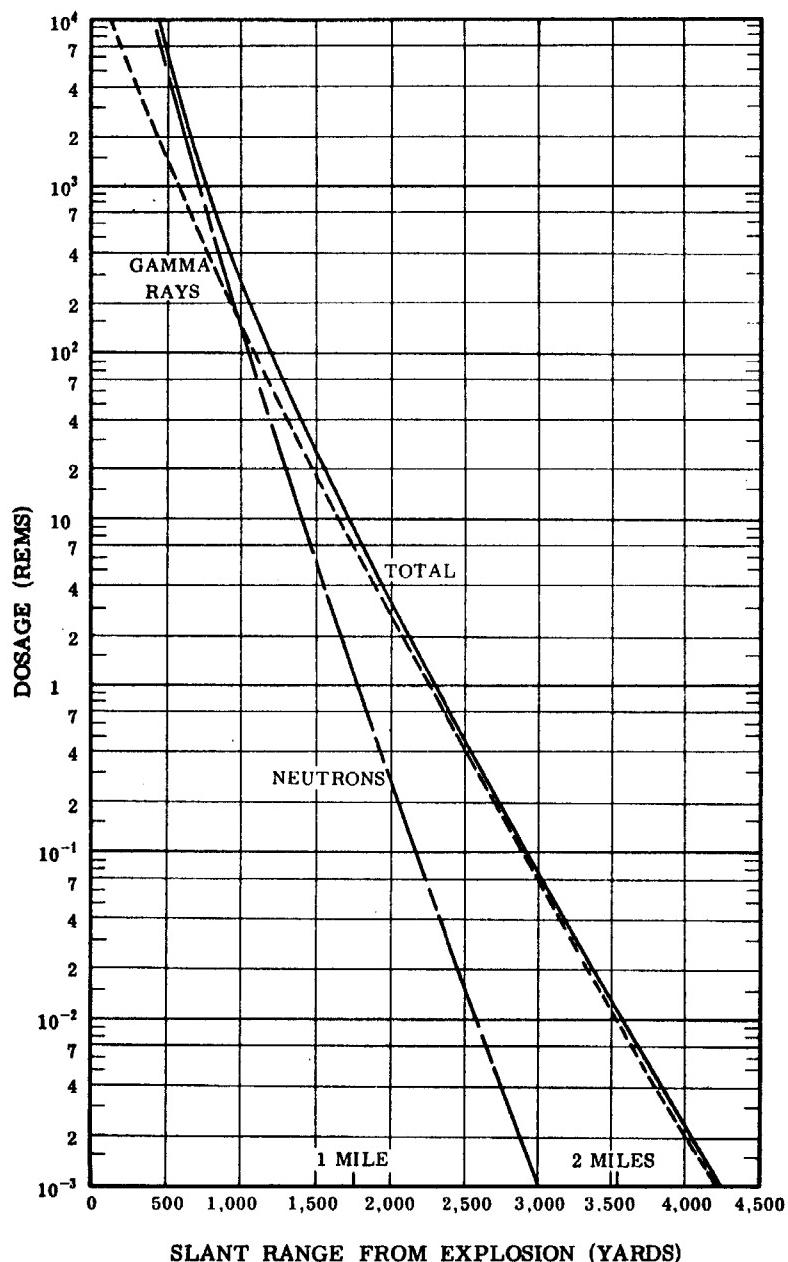


Figure 11.91. Initial gamma-ray and neutron doses as a function of range for a 1-kiloton air burst.

(from Effects of Nuclear Weapons, 1964, p 583)

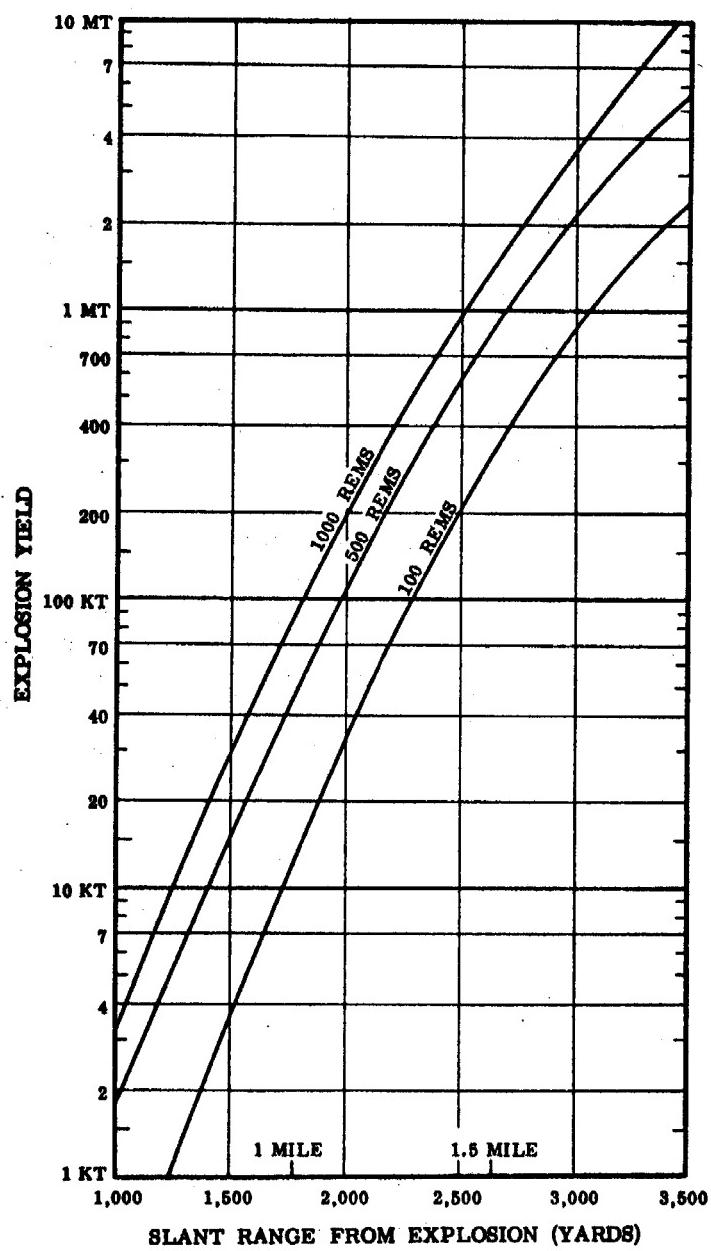


Figure 11.93. Ranges for total doses of 100, 500, and 1,000 rems of initial nuclear radiation as a function of the energy yield.

(from Effects of Nuclear Weapons, 1964, p 584)

SECTION D - RESIDUAL NUCLEAR RADIATION & FALLOUT

D-1 HEIGHT OF BURST FOR EARLY FALLOUT

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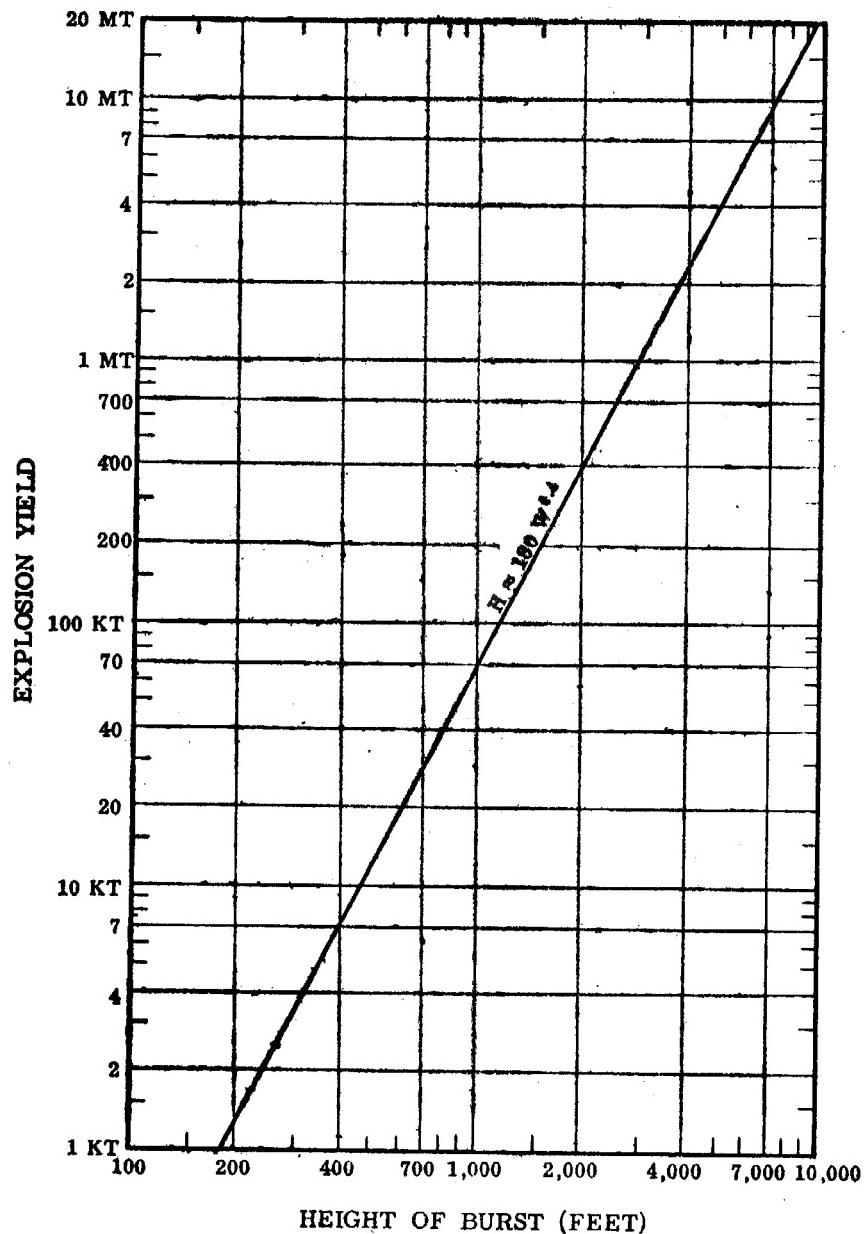


Figure 2.118. Approximate maximum height of burst for appreciable local fallout.

(from Effects of Nuclear Weapons, 1964, p 79)

D - 1

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SECTION D - RESIDUAL NUCLEAR RADIATION & FALLOUT

D-2 DOSE RATE

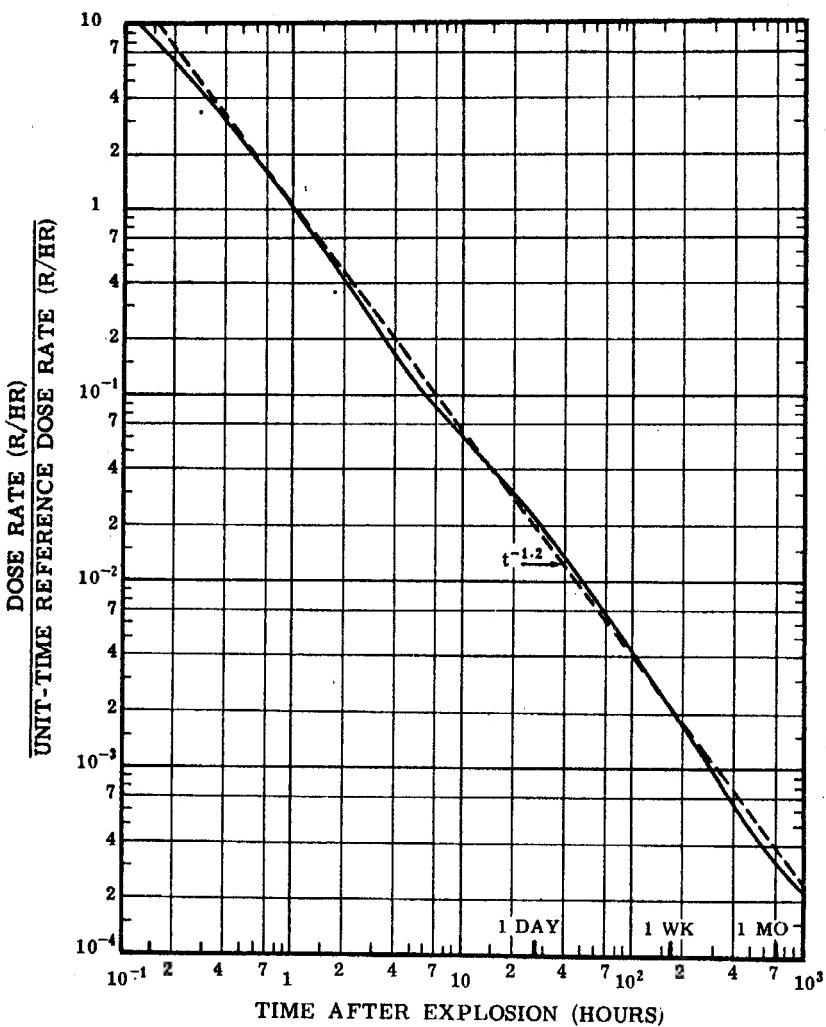


Figure 9.16a. Dependence of dose rate from early fallout upon time after explosion.

(from Effects of Nuclear Weapons, 1964, p 419)

Information concerning the decrease of dose rate in the early fallout can be obtained from the continuous curve in Figs. 9.16a and b, in which the ratio of the approximate exposure dose rate (in R/hr) at any time after burst to a convenient reference value, called the "unit-time reference dose rate", is plotted against time in hours.

EXAMPLE: Suppose that at a given location, the fallout commences at 5 hours after the explosion, and that at 15 hours, when the fallout has ceased to descend, the observed dose rate is 4 R/hr. From the curve in Fig. 9.16a, it is seen that at 15 hours after the explosion the ratio of the actual dose rate to the reference value is 0.04; hence, the reference dose rate must be $4.0/0.04 = 100$ R/hr. By means of this reference value and the decay curves in Figs. 9.16a and b, it is possible to estimate the actual dose rate at the place under consideration at any time after fallout is complete. Thus, if the value is required at 24 hours after the explosion, Fig. 9.16a is entered at

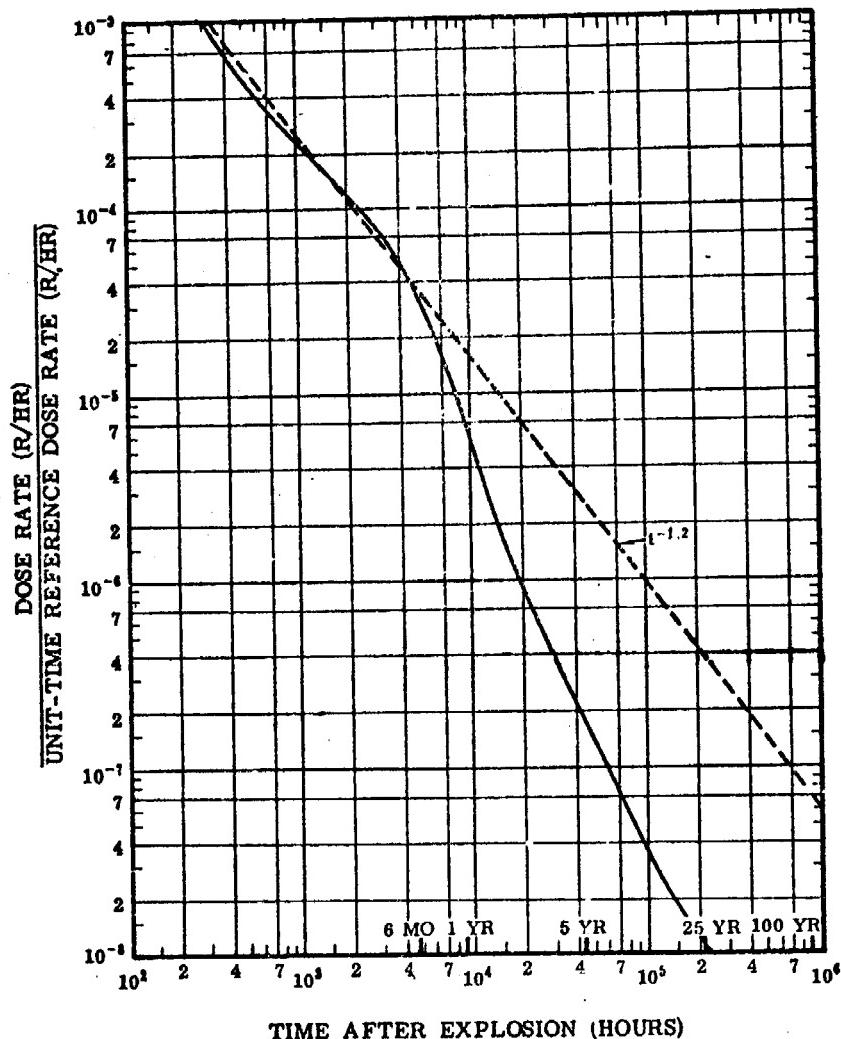


Figure 9.16b. Dependence of dose rate from early fallout upon time after explosion.

(from Effects of Nuclear Weapons, 1964, p 420)

the point representing 24 hours on the horizontal scale. Moving upward until the plotted (continuous) line is reached, it is seen that the required dose rate is 0.023 multiplied by the unit-time reference dose rate, i.e., $0.023 \times 100 = 2.3$ R/hr.

If the dose rate at any time is known, the value at any other time can be estimated.

EXAMPLE: Suppose the dose rate at 3 hours is 50 R/hr; what would be the value at 18 hours? The respective ratios, as given in Fig. 9.16a, are 0.23 and 0.33, with respect to the unit-time reference dose rate. Hence, the dose rate at 18 hours after the explosion is

$$50 \times \frac{0.033}{0.23} = 7.2 \text{ roentgens per hour.}$$

Figure 9.25. Nomograph for calculation of approximate dose rates from early fallout.

The nomograph in Fig. 9.25 gives an approximate relationship between the dose rate at any time after the explosion and the unit-time reference value. If the dose rate at any time is known, that at any other time can be derived from the figure. Alternately, the time after the explosion at which a specific dose rate is attained can be determined approximately.

EXAMPLE:

GIVEN: THE RADIATION dose rate due to fallout at a certain location is 8 roentgens per hour at 6 hours after a nuclear explosion.

FIND: a. The dose rate at 24 hours after the burst.
b. The time after the explosion at which the dose rate is 1 roentgen per hour.

SOLUTION:

Using a straight edge, join the point representing 8 roentgens per hour on the left scale to the time 6 hours on the right scale. The straight line intersects the middle scale at 70 roentgens per hour; this is the unit-time reference value of the dose rate.

a. Using the straight edge, connect this reference point (70 R/hr) with that representing 24 hours after the explosion on the right scale, and extend the line to read the corresponding dose rate on the left scale, i.e.,

1.5 roentgens per hour.

ANSWER

b. Extend the straight line joining the dose rate of 1 R/hr on the left scale to the reference value of 70 R/hr on the middle scale out to the right scale.

This is intersected at 34 hours. ANSWER

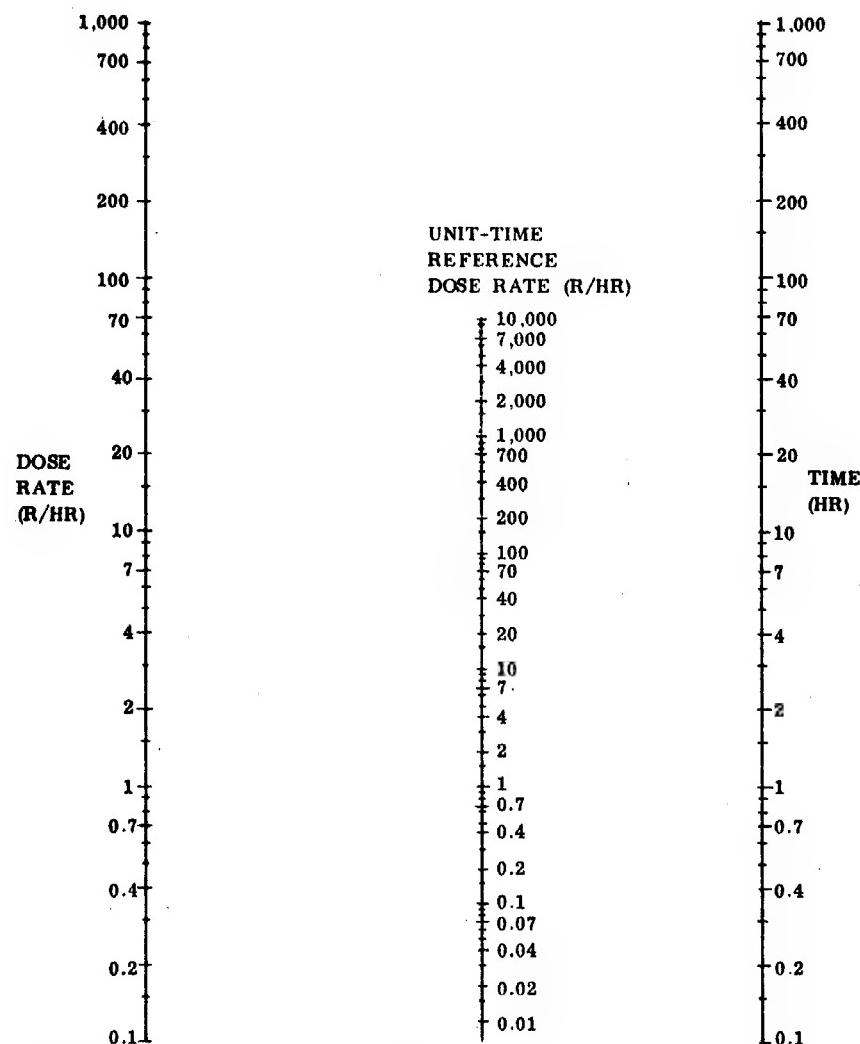


Figure 9.25. Nomograph for calculation of approximate dose rates from early fallout.

(from Effects of Nuclear Weapons, 1964, p 427)

SECTION D - RESIDUAL NUCLEAR RADIATION & FALLOUT

D-3 TOTAL DOSE

Entry Time - Stay Time - Total Dose NomogramEXAMPLE 1: (total dose)

GIVEN: The dose rate in an area at H + 8 is 10 R/hr.

FIND: The total dose received if a person enters this area at H + 10 and remains for four hours.

SOLUTION:

Find the dose rate at H + 1 (120 R/hr) as described in Section D-2. Using a straight edge, connect four hours on the "Stay Time" scale with 10 hours on the "Entry Time" scale. Find .21 on the " D/R_1 " scale. Connect .21 on this scale with 120 R/hr on the "Dose Rate at H + 1" scale. Read the answer from the "Total Dose" scale.

25 R ANSWER

EXAMPLE 2: (entry time)

GIVEN: Dose rate in an area at H + 10 is 12 R/hr. Stay time is 8 hours and the mission dose is established at 50 R.

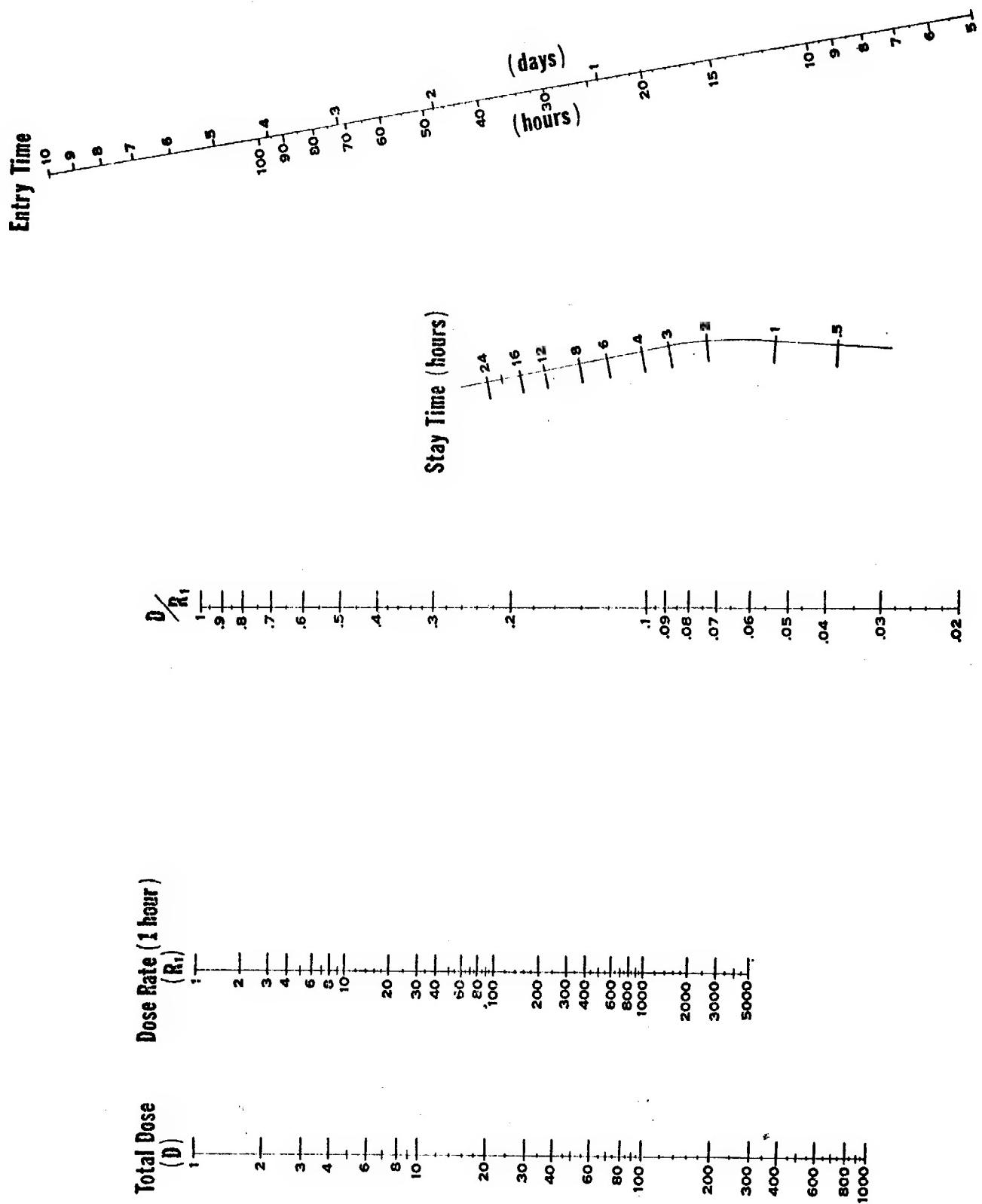
FIND: The earliest entry time into the area.

SOLUTION:

Find the dose rate at H + 1 (190 R/hr). Using a straight edge, connect 50 R on the "Total Dose" scale with 190 R/hr on the "Dose Rate at H + 1" scale. Find .26 on the " D/R_1 " scale. Connect this point (.26) with 3 hours on the "Stay Time" scale. Read the answer from the "Entry Time" scale.

14 hours ANSWER

ENTRY TIME - STAY TIME - TOTAL DOSE
NOMOGRAM



(from Handbook for Radiological Monitors, 1963, DOD, OCD)

Figure 9.26: Total radiation dose from early fallout based on unit-time reference dose rate.

From Fig. 9.26 the total radiation dose received from early fallout during any specified stay in a contaminated area can be estimated if the dose rate at some definite time after the explosion is known. Alternatively, the time can be calculated for commencing an operation requiring a specified stay and a prescribed total radiation dose.

EXAMPLE:

GIVEN: The dose rate at 4 hours after a nuclear explosion is 6 roentgens per hour.

FIND: a. The total dose received during a period of 2 hours commencing at 6 hours after the explosion.

b. The time after the explosion when an operation requiring a stay of 5 hours can be started if the total dose is to be 4 roentgens.

SOLUTION:

The first step is to determine the unit-time reference dose rate (32 roentgens per hour).

a. Enter Fig. 9.26 at 6 hours after the explosion (horizontal scale) and move up to the curve representing a stay time of 2 hours. The corresponding reading on the vertical scale, which gives the multiplying factor to convert unit-time reference dose rate to the required total dose, is seen to be 0.19. Hence, the total dose received is

$$0.19 \times 32 = 6.1 \text{ roentgens} \quad \text{ANSWER}$$

b. Since the total dose is given as 4 roentgens and the unit-time reference dose rate is 32 roentgens per hour, the multiplying factor is $4/32 = 0.125$. Entering Fig. 9.26 at this point on the vertical scale and moving across until the (interpolated) curve for 5 hours stay is reached, the corresponding reading on the horizontal scale, giving the time after explosion, is seen to be

21 hours

ANSWER'

Figure 9.27. Total radiation dose from early fallout based on dose rate at time of entry.

From the chart in Fig. 9.27, the total radiation dose received from early fallout during any specified stay in a contaminated area can be estimated if the dose rate at the time of entry into the area is known. Alternatively, the time of stay may be evaluated if the total dose is prescribed.

EXAMPLE:

GIVEN: Upon entering a contaminated area at 12 hours after a nuclear explosion the dose rate is 5 roentgens per hour.

FIND: a. The total radiation dose received for a stay of 2 hours.
b. The time of stay for a total dose of 20 roentgens.

SOLUTION:

- a. Start at the point on Fig. 9.27 representing 12 hours after the explosion on the horizontal scale and move up to the curve representing a time of stay of 2 hours. The multiplying factor for the dose rate at the time of entry, as read from the vertical scale, is seen to be 1.9. Hence, the total dose received is

$$1.9 \times 5 = 9.5 \text{ roentgens}$$

ANSWER

- b. The total dose is 20 roentgens and the dose rate at the time of entry is 5 roentgens per hour; hence, the multiplying factor is $20/5 = 4.0$. Enter Fig. 9.27 at the point corresponding to 4.0 on the vertical scale and move horizontally to meet a vertical line which starts from the point representing 12 hours after the explosion on the horizontal scale. The two lines are found to intersect at a point indicating a time of stay of about

$$4\frac{1}{2} \text{ hours}$$

ANSWER

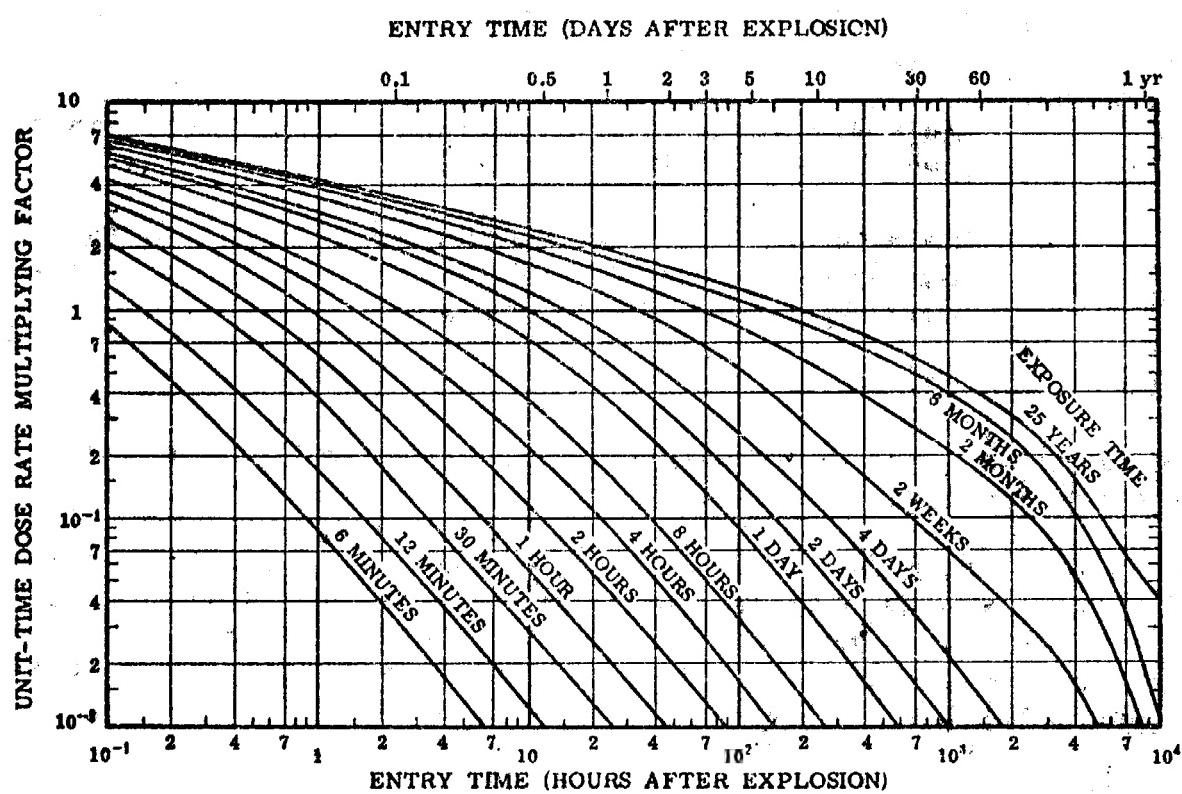


Figure 9.26. Total radiation dose from early fallout based on unit-time reference dose rate.

(from Effects of Nuclear Weapons, 1964, p 429)

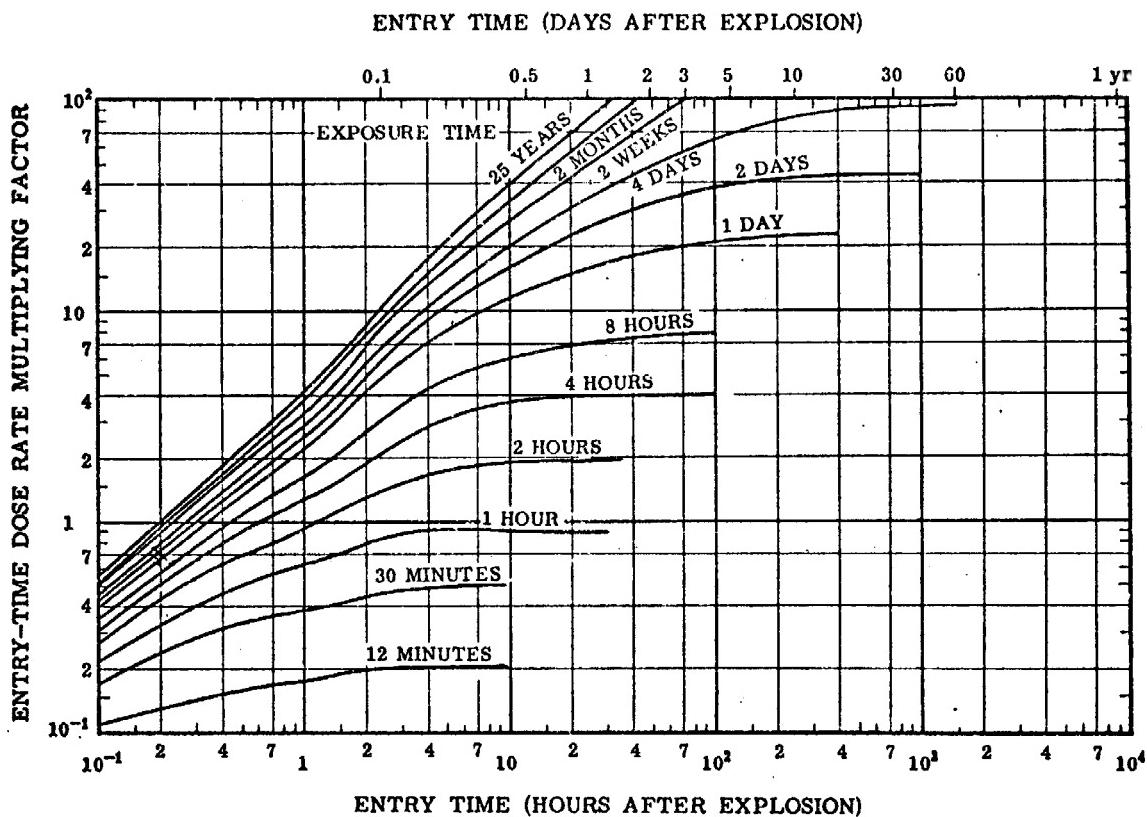


Figure 9.27. Total radiation dose from early fallout based on dose rate at time of entry.

(from Effects of Nuclear Weapons, 1964, p 431)

SECTION E - USEFUL RELATIONSHIPS

E-1 POWERS OF NUMBERS

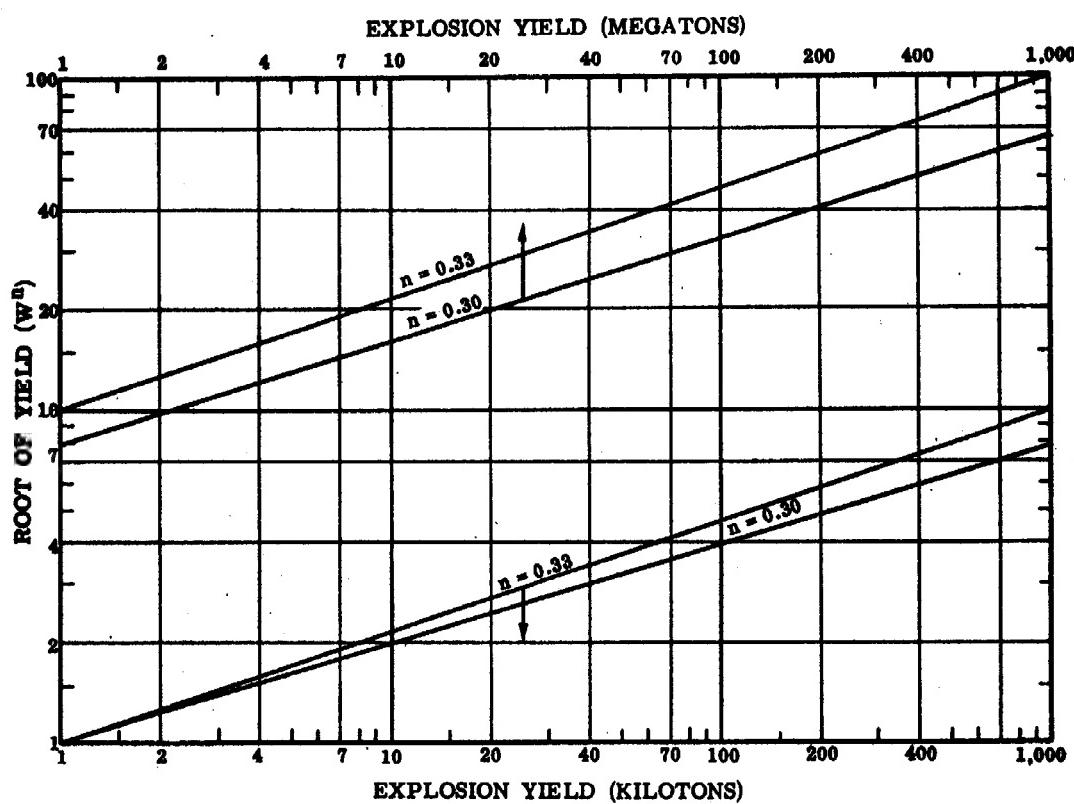


Figure 3.65. Values of $W^{0.33}$ ($W^{1/3}$) and $W^{0.3}$ for use in scaling calculations.

(from Effects of Nuclear Weapons, 1964, p 131)

USEFUL RELATIONSHIPS

POWERS OF NUMBERS

E-1

NUMBER	0.25 POWER	CUBE ROOT	0.4 POWER	0.5 POWER OR SQUARE ROOT
0.5	0.84	0.794	0.758	0.707
1	1.00	1.00	1.00	1.00
2	1.19	1.26	1.32	1.41
4	1.41	1.59	1.74	2.00
6	1.56	1.82	2.05	2.45
8	1.68	2.00	2.30	2.83
10	1.78	2.15	2.51	3.16
12	1.86	2.29	2.70	3.46
14	1.93	2.41	2.88	3.74
15	1.97	2.47	2.96	3.87
16	2.00	2.52	3.03	4.00
17	2.03	2.57	3.11	4.12
18	2.06	2.62	3.18	4.24
20	2.12	2.71	3.32	4.47
25	2.24	2.92	3.62	5.00
30	2.34	3.11	3.90	5.48
35	2.43	3.27	4.15	5.92
40	2.52	3.42	4.38	6.32
45	2.59	3.56	4.58	6.71
50	2.66	3.68	4.78	7.07
55	2.72	3.80	4.96	7.42
60	2.78	3.91	5.15	7.75
65	2.84	4.02	5.31	8.06
70	2.90	4.12	5.47	8.37
75	2.94	4.22	5.63	8.66
80	2.99	4.31	5.77	8.94
85	3.04	4.40	5.91	9.22
90	3.08	4.48	6.05	9.49
95	3.12	4.56	6.18	9.75
100	3.17	4.64	6.30	10.0
110	3.24	4.79	6.56	10.5
120	3.31	4.93	6.80	11.0
130	3.38	5.07	7.00	11.4
140	3.44	5.19	7.22	11.8
150	3.50	5.31	7.42	12.3
155	3.53	5.37	7.50	12.5
160	3.56	5.42	7.62	12.7
165	3.58	5.48	7.70	12.9
170	3.61	5.54	7.80	13.0
175	3.64	5.59	7.90	13.2
200	3.76	5.85	8.33	14.1
250	3.98	6.30	9.10	15.8
300	4.16	6.69	9.80	17.3
350	4.33	7.05	10.4	18.7
400	4.46	7.37	11.0	20.0
450	4.60	7.66	11.5	21.2
500	4.73	7.94	12.0	22.4
550	4.85	8.19	12.5	23.5
600	4.95	8.43	12.9	24.5
650	5.05	8.66	13.4	25.5

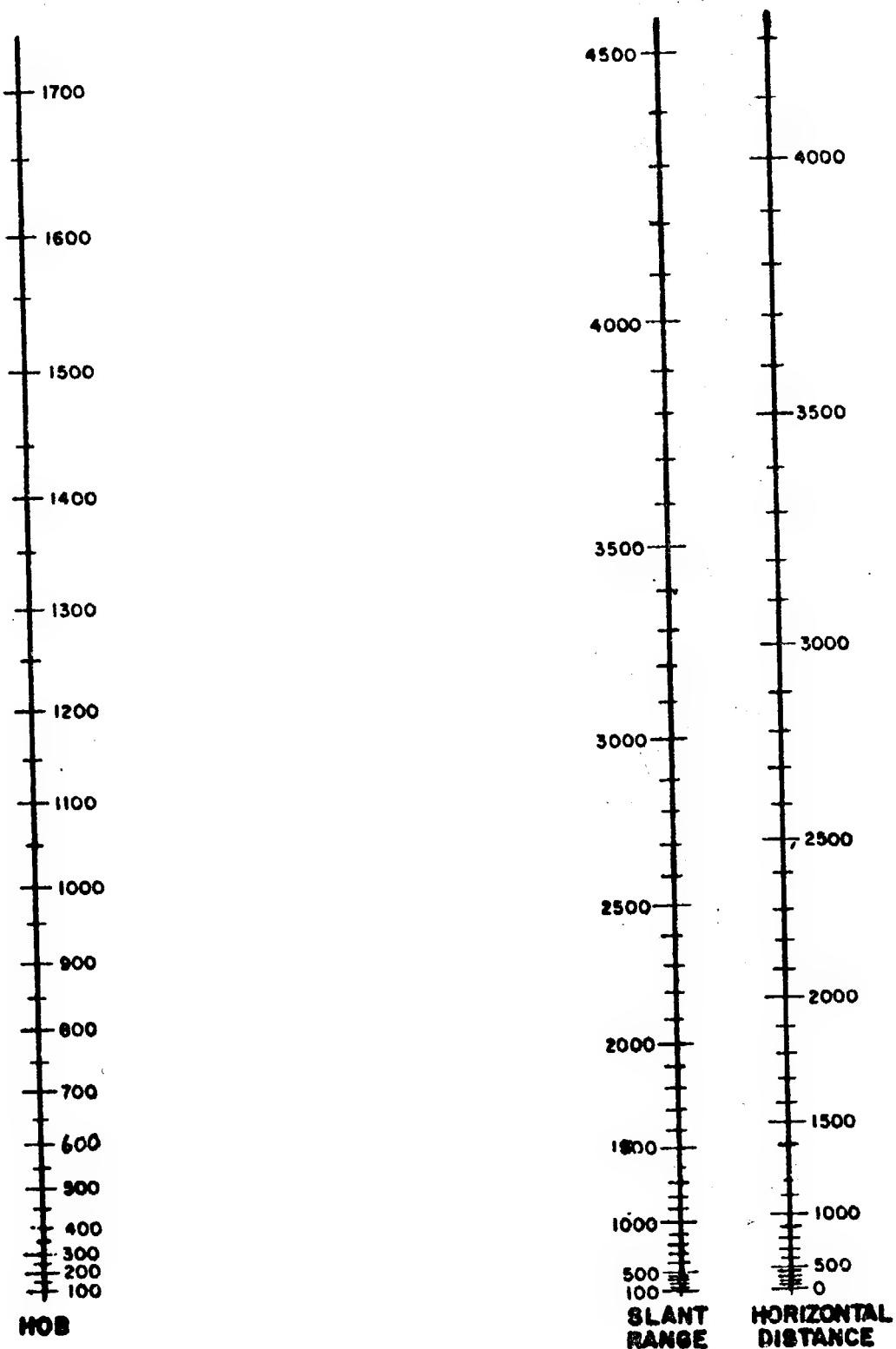
NUMBER	0.25 POWER	CUBE ROOT	0.4 POWER	0.5 POWER OR SQUARE ROOT
700	5.14	8.88	13.8	26.5
750	5.25	9.09	14.2	27.4
800	5.31	9.28	14.5	28.3
850	5.40	9.47	14.9	29.2
900	5.47	9.65	15.3	30.0
950	5.55	9.83	15.5	30.8
1,000	5.61	10.0	15.9	31.6
1,200	5.90	10.6	17.1	34.6
1,400	6.10	11.2	18.1	37.4
1,600	6.30	11.7	19.2	40.0
1,800	6.50	12.2	20.0	42.4
2,000	6.69	12.6	20.9	44.7
2,200	6.85	13.0	21.8	46.9
2,400	7.00	13.4	22.5	49.0
2,600	7.10	13.8	23.3	51.0
2,800	7.30	14.1	23.9	52.9
3,000	7.40	14.4	24.6	54.8
3,200	7.50	14.7	25.3	56.6
3,400	7.60	15.1	25.8	58.3
3,600	7.75	15.3	26.4	60.0
3,800	7.90	15.6	27.0	61.6
4,000	7.94	15.9	27.6	63.3
4,200	8.05	16.1	28.2	64.8
4,400	8.10	16.4	28.6	66.3
4,600	8.20	16.6	29.2	67.8
4,800	8.30	16.9	29.6	69.3
5,000	8.40	17.1	30.2	70.7
5,200	8.50	17.3	30.7	72.1
5,400	8.55	17.6	31.0	73.5
5,600	8.65	17.8	31.5	74.8
5,800	8.75	18.0	32.0	76.2
6,000	8.80	18.2	32.5	77.5
6,500	9.00	18.7	33.5	80.6
7,000	9.15	19.1	34.5	83.7
7,500	9.30	19.6	35.5	86.6
8,000	9.40	20.0	36.5	89.4
8,500	9.60	20.4	37.3	92.2
9,000	9.70	20.8	38.2	94.9
9,500	9.90	21.2	39.0	97.5
10,000	10.00	21.5	39.9	100.
11,000	10.20	22.2	41.4	105.
12,000	10.50	22.9	43.0	110.
13,000	10.70	23.5	44.2	114.
14,000	10.90	24.1	45.6	118.
15,000	11.00	24.7	47.0	122.
16,000	11.20	25.2	48.0	126.
17,000	11.40	25.7	49.0	130.
18,000	11.60	26.2	50.4	134.
19,000	11.80	26.7	51.5	138.
20,000	11.90	27.1	52.5	141.

SECTION E - USEFUL RELATIONSHIPS

E-2 CONVERSION TABLES

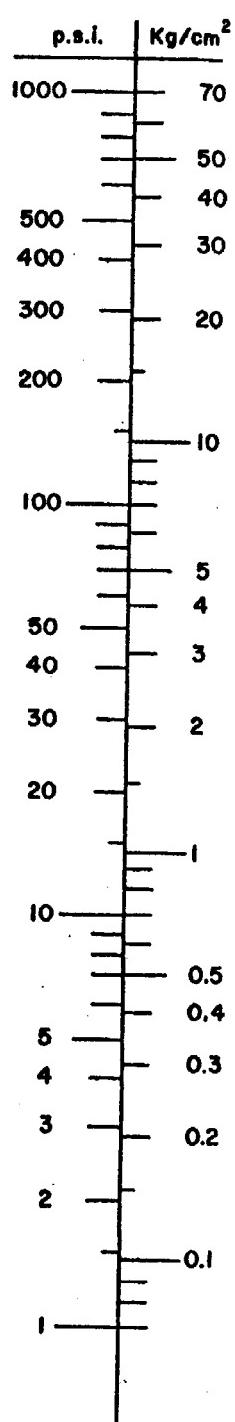
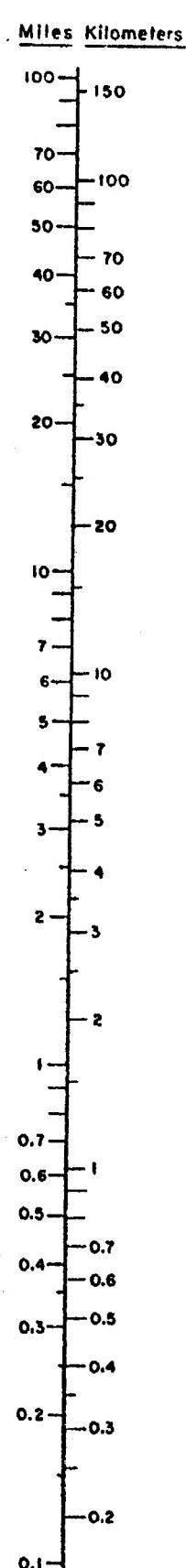
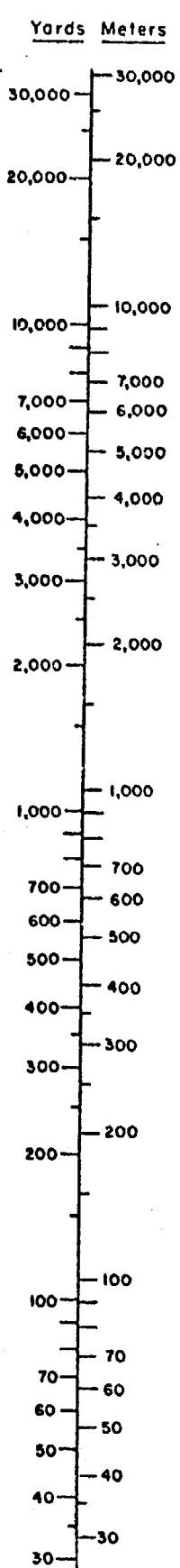
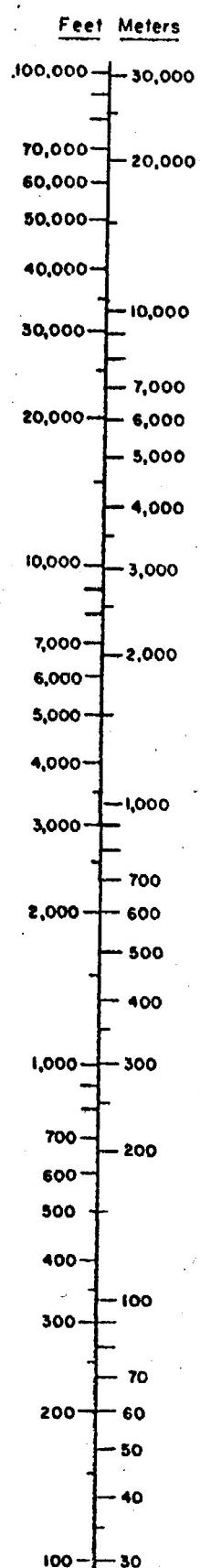
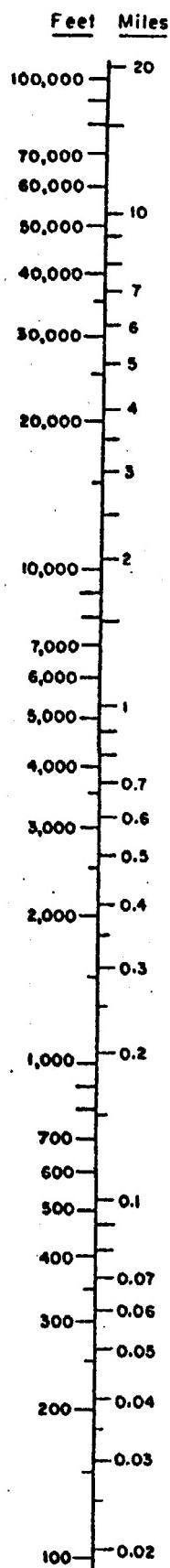
Slant Range - Horizontal Distance Conversion ChartNOTES:

1. As a general rule, conversion of Slant Range and Horizontal Distance is required when either of these distances is equal to or less than three times the Height of Burst.
2. The same unit of measure must be used for all distances; e.g., if HOB and Slant Range are expressed in meters, the Horizontal Distance is also in meters.
3. Where distances are greater than those shown, divide all known values by 2, 3, or any other number and use nomogram in normal manner. Value read from nomogram must then be multiplied by the same number.

SLANT RANGE - HORIZONTAL DISTANCECONVERSION CHART

CONVERSION TABLES

USEFUL RELATIONSHIPS



CONVERSION FACTORS

To convert from	To	Multiply by
Acres	Square feet	43 560
	Square meters	4 , 047
	Square miles	0 . 001563
	Square yards	4 840
Atmospheres	Pounds per square foot	2 , 116 . 3
	Pounds per square inch	14 . 696
Btu	Calories	252
Btu/ft ²	Cal/cm ²	. 271
Calories	Btu	3 . 968 x 10 ⁻³
	Btu/ft ²	3 . 690
Centimeters	Inches	0 . 3937
Cubic feet	Cubic meters	0 . 028317
	Kilograms air	0 . 0347
Cubic meters	Kilograms air	1 . 226
	Cubic feet	35 . 335
Curies	Disintegrations per minute	2 . 2 x 10 ¹²
	Disintegrations per second	3 . 7 x 10 ¹⁰
Disintegrations per minute	Picocuries	0 . 450
Disintegrations per minute per square foot	Millicuries per square mile	0 . 01256
Disintegrations per minute per liter	Microcuries per cubic centimeter	0 . 45 x 10 ⁻⁹
Feet	Meters	0 . 3048
	Miles	0 . 000189
Feet per second	Miles per hour	0 . 68184
Grams	Pounds	0 . 0022046

CONVERSION FACTORS

To convert from	To	Multiply by
Grams per square centimeter	Pounds per square inch	0.014223
Inches	Centimeters	2.54
Kilograms	Pounds	2.2046
Kilograms air	Cubic feet	28.8
Kilograms air	Cubic meters	0.816
Kilograms per square centimeter	Pounds per square inch	14.223
Kilometers	Miles	0.621
Liquid quarts (US)	Liters	0.946
Liters	Liquid quarts (US)	1.057
Meters	Feet	3.28
Microcuries per cubic centimeter	Disintegrations per minute per liter	2.22×10^9
Microns	Centimeters	1×10^{-4}
Miles (nautical)	Miles (statute)	1.1516
Miles	Feet	5,280
	Kilometers	1.6093
Miles per hour	Feet per second	1.4667
Millicuries per square kilometer	Millicuries per square mile	2.59
Millicuries per square kilometer per centimeter	Picocuries per liter	100
Millicuries per square mile	Millicuries per square kilometer	0.386
	Disintegrations per minute per square foot	79.6

CONVERSION FACTORS

To convert from	To	Multiply by
Millicuries per square mile per inch	Picocuries per liter	15.2
Picocuries	Disintegrations per minute	2.22
Picocuries per liter	Millicuries per square kilometer per cm	0.01
	Millicuries per square mile per inch	0.0657
Pounds	Kilograms	0.45359
Pounds per square inch	Atmospheres	0.06805
	Kilograms per square centimeter	0.07031
Square centimeters	Square feet	0.0010764
Square feet	Square centimeters	929.0
Square inches	Square centimeters	6.452
Square kilometers	Square miles	0.386
Square miles	Acres	640.0
Square miles	Square kilometers	2.59

SECTION E - USEFUL RELATIONSHIPS

E-3 MISCELLANEOUS

(BLANK)

TABLE OF ELEMENTS

ELEMENT	SYM-BOL	AT. NO.	AT. WT.	ELEMENT	SYM-BOL	AT. NO.	AT. WT.
Actinium.....	Ac	89	(227)	Mercury.....	Hg	80	200.59
Aluminum.....	Al	13	26.9815	Molybdenum.....	Mo	42	95.94
Americium.....	Am	95	(243)	Neodymium.....	Nd	60	144.24
Antimony.....	Sb	51	121.75	Neon.....	Ne	10	20.183
Argon.....	Ar	18	39.948	Neptunium.....	Np	93	(237)
Arsenic.....	As	33	74.9216	Nickle.....	Ni	28	58.71
Astatine.....	At	85	(210)	Niobium			
Barium.....	Ba	56	137.34	(columbium)...	Nb	41	92.906
Berkelium.....	Bk	97	(249)	Nitrogen.....	N	7	14.0067
Beryllium.....	Be	4	9.0122	Nobelium.....	No	102	(254)
Bismuth.....	Bi	83	208.980	Osmium.....	Os	76	190.2
Boron.....	B	5	10.811	Oxygen.....	O	8	15.9994
Bromine.....	Br	35	79.909	Palladium.....	Pd	46	106.4
Cadmium.....	Cd	48	112.40	Phosphorus.....	P	15	30.9738
Calcium.....	Ca	20	40.08	Platinum.....	Pt	78	195.09
Californium....	Cf	98	(251)	Plutonium.....	Pu	94	(242)
Carbon.....	C	6	12.01115	Polonium.....	Po	84	(210)
Cerium.....	Ce	58	140.12	Potassium.....	K	19	39.102
Cesium.....	Cs	55	132.905	Praseodymium...	Pr	59	140.907
Chlorine.....	Cl	17	35.453	Promethium....	Pm	61	(145)
Chromium.....	Cr	24	51.996	Protactinium...	Pa	91	(231)
Cobalt.....	Co	27	58.9332	Radium.....	Ra	88	(226)
Copper.....	Cu	29	63.54	Radon.....	Rn	86	(222)
Curium.....	Cm	96	(247)	Rhenium.....	Re	75	186.2
Dysprosium....	Dy	66	163.50	Rhodium.....	Rh	45	102.905
Einsteinium....	Es	99	(254)	Rubidium.....	Rb	37	85.47
Erbium.....	Er	68	167.26	Ruthenium.....	Ru	44	101.07
Europium.....	Eu	63	151.96	Samarium.....	Sm	62	150.35
Fermium.....	Fm	100	(253)	Scandium.....	Sc	21	44.956
Fluorine.....	F	9	19.9984	Selenium.....	Se	34	78.96
Francium.....	Fr	87	(223)	Silicon.....	Si	14	28.086
Gadolinium....	Gd	64	157.25	Silver.....	Ag	47	107.870
Gallium.....	Ga	31	69.72	Sodium.....	Na	11	22.9898
Germanium.....	Ge	32	72.59	Strontium.....	Sr	38	87.62
Gold.....	Au	79	196.967	Sulfur.....	S	16	32.064
Hafnium.....	Hf	72	178.49	Tantalum.....	Ta	73	180.948
Helium.....	He	2	4.0026	Technetium....	Tc	43	(99)
Holmium.....	Ho	67	164.930	Tellurium.....	Te	52	127.60
Hydrogen.....	H	1	1.00797	Terbium.....	Tb	65	158.93
Indium.....	In	49	114.82	Thallium.....	Tl	81	204.37
Iodine.....	I	53	126.9044	Thorium.....	Th	90	232.038
Iridium.....	Ir	77	192.2	Thulium.....	Tm	69	168.934
Iron.....	Fe	26	55.847	Tin.....	Sn	50	118.69
Krypton.....	Kr	36	83.80	Titanium.....	Ti	22	47.90
Lanthanum....	La	57	138.91	Tungsten.....	W	74	183.85
Lawrencium....	Lw	103	(257)	Uranium.....	U	92	238.03
Lead.....	Pb	82	207.19	Vanadium.....	V	23	50.942
Lithium.....	Li	3	6.939	Xenon.....	Xe	54	131.30
Lutetium....	Lu	71	174.97	Ytterbium....	Yb	70	173.04
Magnesium....	Mg	12	24.312	Yttrium.....	Y	39	88.905
Manganese....	Mn	25	54.9380	Zinc.....	Zn	30	65.37
Mendelevium....	Md	101	(256)	Zirconium.....	Zr	40	91.22

The value in parenthesis is the mass number of the most stable isotope.

GAMMA DOSE RATE AT 1 FOOT:

$$DR_{1\text{ft}} \approx 6 \text{ C.E.} \pm 20\% \text{ R/hr}$$

where C is curies

E is Mev

BETA DOSE RATE AT 1 FOOT:

$$DR_{1\text{ft}} = 200 \text{ C rads/hr}$$

RANGE OF BETA IN AIR:

<u>Energy (Mev)</u>	<u>Range (m)</u>	<u>Energy (Mev)</u>	<u>Range (m)</u>
0.01	0.0022	0.2	0.36
0.02	0.0072	.3	0.65
0.03	0.015	.4	1.0
0.04	0.024	.6	1.8
0.05	0.037	.8	2.8
0.06	0.050	1.0	3.7
0.07	0.064	1.5	6.1
0.08	0.080	2.0	8.4
0.09	0.095	3.0	13.0
0.10	0.11	4.0	16.0
0.15	0.21	5.0	19.0

RANGE OF BETA IN WATER:

<u>Energy (Mev)</u>	<u>R (inches)</u>	<u>Energy (Mev)</u>	<u>R (inches)</u>
0.1	0.007	0.7	0.095
.2	.02	.8	.14
.3	.03	1.0	.15
.4	.045	2	.4
.5	.075	3	.65
.6	.08	4	.95

AREA OF THE EARTH:

	<u>mi²</u>	<u>km²</u>
land	57.467 x 10 ⁶	148.892 x 10 ⁶
oceans & seas	139.369 "	361.059 "
total	196.836	509.951

Latitude band

0-10	17.016 x 10 ⁶	44.084 x 10 ⁶
10-20	16.512 "	42.778 "
20-30	15.516 "	40.198 "
30-40	14.052 "	36.405 "
40-50	12.158 "	31.497 "
50-60	9.884 "	25.607 "
60-70	7.297 "	18.905 "
70-80	4.475 "	11.594 "
80-90	1.508 "	3.908 "

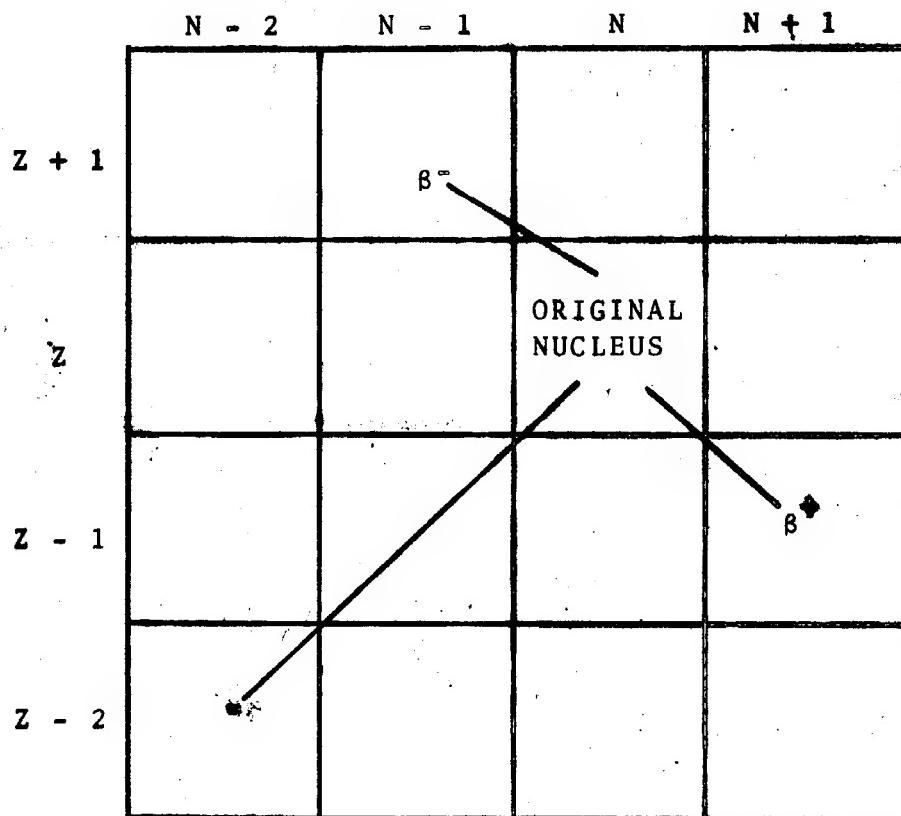
TEMPERATURE/ev:

The temperature associated with 1 ev is:

$$(1.16049 \pm .00005) \times 10^4 \text{ deg (ev)}^{-1}$$

DENSITIES OF COMMON MATERIALS:

	<u>lbs/cu ft</u>	<u>lbs/cu ft</u>	
Brick	120 - 140	Plaster	50 - 180
Concrete	140 - 180	Steel	435 - 495
Reinforced Concrete	140 - 190	Iron	450 - 480
Aluminum	169	Lead	710
Wood: Hard	40 - 55	Copper	550
Soft	30 - 44	Rubber	58
Earth	77 - 120	Glass	160 - 170
Clay:	145	Chalk	145
Sand: Wet	115 - 130	Sandstone	130 - 170
Dry	90 - 110	Limestone	130 - 140
		Granite	165 - 175

DISPLACEMENT IN TABLE OF ELEMENTSCAUSED BY RADIOACTIVE DECAY

N = no. of neutrons

Z = no. of protons

Element is not shifted by emission of gamma radiation.

HALF-LIVES OF SOME RADIONUCLIDES OF INTEREST1. NEUTRON INDUCED ACTIVITIESa. In Air N^{16}

	HALF-LIFE	EMITS	DECAYS TO
--	-----------	-------	-----------

7 secs.

 β γ O^{16} C^{14}

5,700 years

 β N^{14} b. In Soil Na^{24}

15 hours

 β γ Mg^{24} Mn^{56}

2.6 hours

 β γ Fe^{56} Si^{31}

2.6 hours

 β γ P^{31} Al^{28}

2.3 mins.

 β γ Si^{28} Cl^{38}

37 mins.

 β γ Ar^{38} c. Other Zn^{65}

245 days

 β^+ γ Cu^{65} Cu^{64}

13 hours

 β^+ or β^- γ Ni^{64} or Zn^{64} 2. SOME FISSION PRODUCTS Xe^{140}

16 secs.

 β Cs^{140} Cs^{140}

66 secs.

 β Ba^{140} Ba^{140}

13 days

 β γ La^{140} La^{140}

40 hours

 β γ Ce^{140} I^{137}

22 secs.

 β Xe^{137} Xe^{137}

4 mins.

 β Cs^{137}

	HALF-LIFE	EMITS	DECAYS TO
Cs ¹³⁷	30 years	β γ	Ba ¹³⁷
Sn ¹³¹	3.4 mins.	β	Sb ¹³¹
Sb ¹³¹	22 mins.	β	Te ¹³¹
Te ¹³¹	30 hours	β γ	I ¹³¹
I ¹³¹	8 days	β γ	Xe ¹³¹
Kr ⁹⁰	33 secs.	β	Rb ⁹⁰
Rb ⁹⁰	2.7 mins.	β γ	Sr ⁹⁰
Sr ⁹⁰	28 years	β	γ ⁹⁰
γ ⁹⁰	64 hours	β γ	Zr ⁹⁰
Kr ⁸⁹	3.2 mins.	β	Rb ⁸⁹
Rb ⁸⁹	15 mins.	β γ	Sr ⁸⁹
Sr ⁸⁹	54 days	β	γ ⁸⁹
3. OTHERS			
H ³	12 years	β	He ³
Pu ²³⁹	24,300 years	α γ	U ²³⁵
U ²³⁵	7×10^8 years	α γ	Th ²³¹
U ²³⁸	4.5×10^9 years	α γ	Th ²³⁴
Co ⁶⁰	5.2 years	β γ	Ni ⁶⁰

SECTION F - GLOSSARY OF TERMS

This glossary contains a limited selection of terms commonly used on the RSO course. A more comprehensive glossary of technical terms is contained in Effects of Nuclear Weapons, 1964. General terms used throughout the Emergency Measures Organizations in Canada are defined in A Guide to Civil Emergency Planning for Municipalities.

P

GLOSSARY OF TERMS

<u>TERM</u>	<u>DEFINITION</u>
ATOMIC NUMBER (Z)	The number of protons in the nucleus; the number of positive charges on the nucleus; the number of orbital electrons around the nucleus of a neutral atom.
ATOMIC WEIGHT (A)	The weighted mean of the masses of the neutral atoms of an element expressed in atomic weight units.
ATTO-	Prefix meaning 10^{-18} .
AVERAGE LIFE (mean life)	The average of the individual lives of all the atoms of a particular radioactive substance. It is 1.443 times the radioactive half life.
CURIE (Ci, also c)	The quantity of a radioactive nuclide in which the number of disintegrations is 3.700×10^{10} per second.
DOSE (DOSAGE)	The radiation delivered to a specified area or volume, or to the whole body. In recent years there has been an increasing tendency to regard a dose of radiation as the amount of energy absorbed by tissue at the site of interest per unit mass (see "rad") (see also "exposure").
ABSORBED DOSE	The quantity of energy imparted to a mass of material exposed to radiation.
ACCUMULATED DOSE	The total dose resulting from repeated exposures to radiation of the same region or of the whole body.
ACUTE DOSE	A dose of whole body irradiation received in a short time.
MAXIMUM PERMISSIBLE DOSE	The maximum dose of radiation which may be received by persons working with ionizing radiation.
MEDIAN LETHAL DOSE	See LD-50.

GLOSSARY OF TERMS

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TERM

DEFINITION

DOSE RATE

Radiation dose delivered per unit time, e.g. roentgens per hour.

ELECTRON VOLT (ev)

A unit of energy equivalent to the amount of energy gained by an electron in passing through a potential difference of one volt. (Multiples are Kev, Mev, Bev)

EXPOSURE

The product of radiant flux density multiplied by exposure time.

ACUTE EXPOSURE

Radiation exposure of short duration (arbitrarily set, say at 24 hours or some other comparable interval).

CHRONIC EXPOSURE

Radiation exposure of long duration by fractionation or protraction.

FEMTO-

Prefix meaning 10^{-15} .

GIGA-

Prefix meaning one billion, 10^9 .

GROUND ZERO (GZ)

The point on the surface of land, or water, vertically below or above, the centre of burst of a nuclear weapon.

HALF-LIFE, BIOLOGICAL

The time required for the body to eliminate one-half of an administered dose of any substance by regular processes of elimination.

HALF-LIFE, EFFECTIVE

The time required for a radioactive element fixed in the tissue of an animal body to be diminished 50 percent as a result of the combined action of radioactive decay and biological elimination.

$$Eh_1 = \frac{bh_1 \times rh_1}{bh_1 + rh_1}$$

HALF-LIFE, RADIOACTIVE

The time required for a radioactive substance to lose 50 percent of its activity by decay.

GLOSSARY OF TERMS

<u>TERM</u>	<u>DEFINITION</u>
HALF THICKNESS (HALF VALUE LAYER)	The thickness of any particular material that will reduce the intensity of a beam of radiation to half its original value.
ISOTOPE	One of several nuclides having the same atomic number, but different mass numbers. Isotopes are either stable or radioactive.
Kev	Kiloelectron volts; thousand electron volts.
KILO-	Prefix meaning one thousand; 10^3 .
KILOTON (KT)	One thousand tons.
LD-50 (LD ₅₀ ; MLD, MEDIAN LETHAL DOSE)	That dose of a toxic agent which would be expected to kill 50% of a large group of individuals receiving it.
MASS NUMBER (A)	The number of nucleons (protons and neutrons) in the nucleus of an atom.
MEAN FREE PATH	The average distance that a particle travels between successive collisions with other particles.
MEAN LIFE	See "average life".
MEGA-	Prefix meaning one million; 10^6 .
MEGATON (MT)	One million tons.
Mev	One million electron volts.
MICRO-	Prefix meaning one millionth; 10^{-6} .
MICRON	10^{-6} meters.
MILLI-	Prefix meaning one thousandth; 10^{-3} .
NANO-	Prefix meaning one billionth; 10^{-9} .
NOMINAL	Obsolescent designation of 20 KT nuclear weapons.

GLOSSARY OF TERMS

F

<u>TERM</u>	<u>DEFINITION</u>
NUCLEON	A constituent particle of the atomic nucleus.
NUCLIDE	A species of atom characterized by the constitution of its nucleus.
OPTIMUM HEIGHT	The height of burst at which some specified level of damage is at a maximum. (This term has fallen into disuse since the advent of high yield weapons)
PICO-	Prefix for 10^{-12} , e.g. one picocurie = $\frac{1}{1,000,000,000,000}$ curie.
PROTECTION FACTOR (PF)	The relative reduction in the amount of gamma radiation that would be received by an individual in a protected location, compared to the amount he would receive if unprotected.
RAD	Unit of absorbed dose of radiation; one hundred ergs of absorbed energy per gram of absorbing material.
RELATIVE BIOLOGICAL EFFECTIVENESS (RBE)	The ratio of gamma, or X-ray, dose to the dose that is required to produce the same biological effect by the radiation in question.
REM (ROENTGEN EQUIVALENT, MAN)	That quantity of any type of ionizing radiation which, when absorbed by man, produces an effect equivalent to the absorption by man of one roentgen of gamma or X-radiation.
ROENTGEN (R)	The quantity of gamma or X-radiation such that the associated corpuscular emission per 0.001293 gram of air produces, in air, ions carrying one electrostatic unit of electricity of either sign.

GLOSSARY OF TERMS

<u>TERM</u>	<u>DEFINITION</u>
SCALING	Calculating the effects of a specified yield of weapon from the observed effects of a different yield of weapon.
SPECIFIC ACTIVITY	The activity per unit mass of material.
TERA-	Prefix for one million million, 10^{12} .
YIELD	The energy released in a nuclear explosion (usually expressed in tons, kilotons, or megatons, equivalent of TNT).
Z	See "Atomic Number".